# A GA-DE hybrid evolutionary algorithm for path synthesis of four-bar linkage 

Wen-Yi Lin*<br>Department of Mechanical Engineering, De Lin Institute of Technology, 1 Lane 380, Qingyan Road, Tucheng, Taipei County, Taiwan, ROC

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#### Abstract

A new real-coded evolutionary algorithm is proposed for application to path synthesis of a four-bar linkage. This new evolutionary algorithm is obtained by combining differential evolution (DE) with the real-valued genetic algorithm (RGA). We term this the "GA-DE hybrid algorithm." The only difference between the proposed algorithm and RGA is in the content of the crossover. The crossover operation in the RGA is replaced by differential vector perturbation, with the best individual or some excellent individuals as the base vectors. Thus, both the main perturbation of differential vectors and the minor perturbation of mutation are used as genetic operators in the GA-DE hybrid algorithm. The efficiency and accuracy of the proposed method are tested using four cases. Findings show that much more accurate solutions for three cases are obtained with this method than those obtained using other evolutionary methods as discussed in the literature. A moveable stick diagram of the synthesized mechanisms can be obtained using the 2D sketch feature of SolidWorks®. This can be used to check whether the synthesized mechanisms encounter circuit defects or are incapable of motion.


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## 1. Introduction

The path synthesis of a four-bar linkage has been actively studied during the past 50 years. There have been a large number of studies on this topic using a variety of methods. These include analytical [1,2], continuation [3], nonlinear goal programming [4,5], exact gradient [6], coupler-angle function curve [7] and curve curvature methods [8]. The problem of path synthesis of a four-bar linkage is to generate a mechanism whose coupler point can trace the desired trajectory or target points. There is no analytical solution to the general problem of four-bar linkage synthesis for more than five target points. This type of problem may be solved by a variety of numerical methods. For example, it may be considered a mechanism optimization to minimize an objective function. The most common objective function is the so-called position error, defined as the sum of the square of the Euclidean distance between the target points and the obtained coupler points. Following the development of evolutionary algorithms from natural biological evolution and swarm intelligence, the merits of these algorithms are what make them suitable for application to path synthesis of the four-bar linkage. The genetic algorithm (GA) was first introduced by Holland [9], then verified by his student, DeJong [10], as applicable to numerical optimization problems. Differential evolution (DE), first proposed by Storn and Price [11], is another simple yet powerful evolutionary algorithm for real parameter optimization. Particle swarm optimization (PSO), proposed by Kennedy and Eberhart [12], is one of the swarm intelligence optimization methods that operate by imitating the swarming behaviors of natural creatures. These evolutionary methods are simple and easy to implement for solving complicated real-world optimization problems. For these evolutionary methods, there is no need for further demands pertaining to the gradient or other mathematical characteristics of the objective function. Furthermore, if the objective function of an optimization task is not expressed as an explicit function of the design variables, or alternatively, it is too complicated to manipulate, e.g., the

[^0]optimization problem of dimensional synthesis of the five-point double-toggle mold clamping mechanism [13,14], it is more suitable to use these evolutionary algorithms for optimization than the traditional deterministic optimization methods.

Although "genetic algorithm" is used in the title of Ref. [15], Cabrera et al. actually applied a new evolutionary method based on DE to the path synthesis of a four-bar linkage. However, their method is somewhat different than either GA or DE. The main difference between the new evolutionary method and DE is the mutation operation in GA retained in the new evolutionary method. The objective function has two parts. The first part is concerned with the position error. In the second part the constraints are inserted by the penalty function. Three cases were studied. The solutions of two cases were compared with those obtained by Kunjur and Krishnamurty [16] based on the deterministic and genetic methods. Findings show that quite small errors in fast convergence are obtained and therefore the new evolutionary algorithm is relatively effective and efficient. Notice that the final error for case 2 obtained by Cabrera et al. is the same as the position error for their synthesized parameters. However, the values of the final errors for cases 1 and 3 are not the same. Alternatively, the errors for cases 1 and 3 obtained by Cabrera et al. might be incorrect or typing errors. To find the best algorithm among binary-coded GA (BGA), PSO and DE, Acharyya and Mandal [17] applied BGA with multipoint crossover, the PSO with the CFA (constriction factor approach) and the DE with DE/rand/1/exp strategy to the path synthesis of a four-bar linkage. They also introduced a new refinement technique for the generation of initial population. This technique is quite helpful for solving the constrained optimization problem. Three cases were studied for more than five target points. Findings show that the DE method produces a better solution than that obtained previously by Cabrera et al. for case 1, and DE outperforms BGA and PSO for all three cases. However, some of their results for cases 2 and 3 might be unreliable. The error for case 1 obtained by Cabrera et al. has been corrected by Acharyya and Mandal. Notice again that the error employed by Acharyya and Mandal is the square root of the position error. However, this is not clearly stated. The error for the BGA solution for case 2 and the errors for the BGA, PSO and DE solutions for case 3 might be incorrect or alternatively, their synthesized parameters might be typing errors. If the synthesized parameters shown in their paper are correct, the error for the BGA solution for case 2 should be 45.817 , not 3.171 (according to their synthesized parameters). The errors for the BGA, PSO and DE solutions for case 3 should be 2.403, 37.083 and 50.423, respectively, not 2.281, 1.971 and 1.952 (according to their synthesized parameters).

The aim of this work is to propose a new real-valued evolutionary algorithm to apply to the path synthesis problems of the four-bar linkage. The new evolutionary algorithm is a combination of the real-valued genetic algorithm (RGA) and the differential evolution. Accordingly, this algorithm will be termed "GA-DE hybrid (evolutionary) algorithm." To verify the efficiency and accuracy of the proposed method, several of the afore-mentioned cases are studied. The only difference between the proposed evolutionary algorithm and the real-valued genetic algorithm is in the content of the crossover. The crossover operation in RGA is replaced by the differential vector perturbation of DE [18], with the best individual or some excellent individuals as the base vectors. Thus, both the main perturbation of the differential vectors and the minor perturbation of the mutation act as genetic operators in the proposed evolutionary algorithm.

It has been pointed out [19] that the synthesized solution may be unusable due to circuit or order defects, or be incapable of moving from one coupler point to another. Although a synthesized solution can be at the traced points, there is no guarantee regarding the behavior of the linkage between those traced points. A circuit defect occurs when the linkage cannot move into a region between those traced points, that is, positions do not exist in such this region for a linkage with a circuit defect. Therefore, a linkage with a circuit defect must be disassembled before the region and reassembled after the region to complete the motion. This is a fatal defect. In this work, a 2D sketch produced by SolidWorks ${ }^{\circledR}$ is used to check whether the synthesized mechanism encounters such defects. One can manipulate rotations of the driving link of the SolidWorks ${ }^{\circledR} 2 \mathrm{D}$ sketch for the synthesized linkage by using the mouse to drag the driving link to produce the motion. If the driving link cannot be dragged into a region, this indicates the presence of a circuit defect. If one compels the driving link to complete the motion in the 2D sketch, one can observe the phenomenon of jumping between the two limiting positions. Besides, if the defect leading to incapable of movement is not the result of the circuit defect, the driving link cannot be compelled to move in the 2D sketch. The 2D sketch is also helpful to examine the distance between the target point and the synthesized coupler point obtained from the synthesized geometric parameters and the position equations.

## 2. Problem formulation

### 2.1. Position equations

Fig. 1 depicts a skeleton drawing and all the geometric parameters of the four-bar linkage, where $C$ is the coupler point. The DOF of the four-bar linkage is one. Angle $\theta_{2}$ is the input angle in this work and angle $\theta_{3}$ can be solved by the Freudenstein equation [20]. The position of coupler point $C$ in the world coordinate system $O X Y$ can be expressed by

$$
\left[\begin{array}{l}
C_{X}  \tag{1}\\
C_{Y}
\end{array}\right]=\left[\begin{array}{cc}
\cos \theta_{0} & -\sin \theta_{0} \\
\sin \theta_{0} & \cos \theta_{0}
\end{array}\right]\left[\begin{array}{l}
C_{X r} \\
C_{Y r}
\end{array}\right]+\left[\begin{array}{l}
x_{0} \\
y_{0}
\end{array}\right]
$$

where

$$
\begin{align*}
& C_{X r}=r_{2} \cos \theta_{2}+r_{c x} \cos \theta_{3}-r_{c y} \sin \theta_{3}  \tag{2}\\
& C_{Y r}=r_{2} \sin \theta_{2}+r_{c x} \sin \theta_{3}+r_{c y} \cos \theta_{3}
\end{align*}
$$



Fig. 1. Four-bar mechanism in the global coordinate system.

### 2.2. Design parameters

There are at least nine design parameters for path generation with prescribed timing, $r_{1}, r_{2}, r_{3}, r_{4}, r_{c x}, r_{c y}, x_{0}, y_{0}$ and $\theta_{0}$ to be optimized. In addition to the nine design parameters, there are input angles $\theta_{2}^{i}(i=1-N)$ corresponding to target points that need to be optimized for path generation without prescribed timing. Design variable vector $\mathbf{X}$ is given as follows:

$$
\begin{equation*}
\mathbf{X}=\left[r_{1}, r_{2}, r_{3}, r_{4}, r_{c x}, r_{c y}, x_{0}, y_{0}, \theta_{0}, \theta_{2}^{1}, \theta_{2}^{2} \ldots \theta_{2}^{N}\right] \tag{3}
\end{equation*}
$$

where $N$ is the number of target points to be optimized.

### 2.3. Design objective

The position error is defined as the sum of the square of the Euclidean distance between each $C_{d}^{i}$ and the corresponding $C^{i}$, where $\left\{C_{d}^{i}\right\}$ is the set of the positions of target points (indicated by the designer); and $\left\{C^{i}\right\}$ is the set of the positions of the coupler point of the synthesized mechanism for a set of input angles $\left\{\theta_{2}^{i}\right\}$. They can be written in the world coordinate system as $\mathbf{C}_{d}^{i}=\left[C_{X d}^{i}\right.$, $\left.C_{Y d}^{i}\right]^{T}$ and $\mathbf{C}^{i}=\left[C_{X}^{i}, C_{Y}^{i}\right]^{T}$, respectively.

In this work, the four-bar linkage synthesized problem is to minimize the position error considered as the first part of the objective function, which may be expressed by

$$
\begin{equation*}
f_{\mathrm{obj}}=\sum_{i=1}^{N}\left[\left(C_{X d}^{i}-C_{X}^{i}(\mathbf{X})\right)^{2}+\left(C_{Y d}^{i}-C_{Y}^{i}(\mathbf{X})\right)^{2}\right] \tag{4}
\end{equation*}
$$

For the establishment of a termination criterion, the mean error in distance between the target and coupler points is defined as

$$
\begin{equation*}
e_{\mathrm{m}}=\frac{1}{N} \sum_{i=1}^{N} \sqrt{\left(C_{X d}^{i}-C_{X}^{i}(\mathbf{X})\right)^{2}+\left(C_{Y d}^{i}-C_{Y}^{i}(\mathbf{X})\right)^{2}} \tag{5}
\end{equation*}
$$

### 2.4. Constraints

In this study, only the following constraints are considered:

1. the Grashof condition is satisfied to allow for the entire turn of at least one link. It may be expressed by

$$
\begin{equation*}
2\left[\max \left(r_{1}, r_{2}, r_{3}, r_{4}\right)+\min \left(r_{1}, r_{2}, r_{3}, r_{4}\right)\right]<\left(r_{1}+r_{2}+r_{3}+r_{4}\right) \tag{6}
\end{equation*}
$$

2. The sequence of input angles $\theta_{2}$ satisfies CW or CCW rotation of the crank.
3. The design parameters are within the specified ranges.
4. The rotation range of the crank.

For all cases discussed here, the crank has $360^{\circ}$ of rotation (constraint 4). Apart from the input angles, constraint 3 may be achieved by assigning the value of a design variable within the prescribed range during initialization and mutation operations. Furthermore, if the value obtained by crossover operation is not within the prescribed range, one may repeat this operation until the value falls within the prescribed range. The input angles are assigned values within the range $[0,2 \pi]$ only during initialization and mutation operations. If the obtained input angle exceed its limit, say $2 \pi<\theta_{2}<4 \pi$, the final value is obtained by subtraction of $2 \pi$
from the obtained value. Therefore, it is allowable for the value of the input angle to exceed its limit during the course of evolution, so long as constraint 2 is satisfied in the final evolution. Furthermore, by rearranging the input angles to satisfy CW or CCW rotation during initialization and mutation operations, constraint 2 may be ignored until the end of the evolution. Sound chromosomes may be obtained both by this scheme and the mechanism of evolution. The scheme proposed in this work differs from that proposed by Acharyya and Mandal, in that their scheme is carried out only in the process of initialization and their algorithm always checks constraints 2 in each generation. Lastly constraint 1 is inserted into the objective function as a penalty function as follows:

## Minimize

$$
\begin{equation*}
f_{\mathrm{obj}}=\sum_{i=1}^{N}\left[\left(C_{X d}^{i}-C_{X}^{i}(\mathbf{X})\right)^{2}+\left(C_{Y d}^{i}-C_{Y}^{i}(\mathbf{X})\right)^{2}\right]+M_{1} h_{1}(\mathbf{X}) \tag{7}
\end{equation*}
$$

where $h_{1}(\mathbf{X})=0$ indicates that Grashof's condition is true and $h_{1}(\mathbf{X})=1$ indicates that Grashof's condition is false; $M_{1}$ is a constant with a very large value that penalizes the objective function when the constraint fails.

## 3. GA-DE hybrid evolutionary algorithm

The GA-DE hybrid evolutionary algorithm is obtained by combining the real-valued genetic algorithm with the differential evolution. Genetic algorithms are global search techniques based on the concepts of genetics, natural selection and survival of the fittest. The RGA search process is briefly outlined below. A population with randomly generated chromosomes is initialized. Each chromosome (individual) is a candidate solution. The quality of the individual is estimated by the fitness value related to the objective function. Offsprings are generated using genetic operators, crossover and mutation, from either one or two individuals (parents). The parents are randomly selected according to a probability proportional to their fitness. A population evolves from generation to generation by selection pressure and genetic operations.

There are several methods of crossover in RGA, such as arithmetic crossover [21] and blend crossover (BLX- $\alpha$ ) [22]. However, these RGA methods do not necessarily work better than those of BGA for the problem of linkage synthesis. There exist a number of other crossover operations, for example, simulated binary crossover [23,24] and fuzzy recombination operations [25]. Beyer and Deb [26] found there to be some similarity in such crossover methods. As pointed out in [27], crossover using such methods is not as meaningful in RGA when contrasted with crossover in BGA. Crossover operators in RGA may be best described as blending operators and may be regarded as perturbations. Most blending operators in RGA are known as crossover operators. Furthermore, although debatable, Deb believes that the distinction between the crossover and mutation operations in RGA lies mainly in the number of individuals used in the perturbation process. We agree with Deb's opinion, so in this work, the crossover is replaced by a differential vector perturbation of $D E$ evolution. Thus, both the main perturbation of differential vectors and the minor perturbation of mutation which act as genetic operators are used in the proposed evolutionary algorithm.

Here, genes $x_{i}(i=1-n)$ represent the design parameters encoded in terms of real numbers that fall between their bounds. All genes are grouped in a vector $\mathbf{X}$ that represents a chromosome. That is

$$
\begin{align*}
& x_{i} \in\left[\min \left(x_{i}\right), \max \left(x_{i}\right)\right]  \tag{8}\\
& \mathbf{X}=\left[x_{1}, x_{2}, \ldots, x_{n}\right]=\left[r_{1}, r_{2}, r_{3}, r_{4}, r_{c x}, r_{c y}, x_{0}, y_{0}, \theta_{0}, \theta_{2}^{1}, \theta_{2}^{2} \ldots \theta_{2}^{N}\right] \tag{9}
\end{align*}
$$

where $n$ is the number of the design parameters.

### 3.1. Initialization

An initial population with $N_{\mathrm{p}}$ chromosomes is randomly generated. The gene in each chromosome is given by

$$
\begin{equation*}
x_{i}=\min \left(x_{i}\right)+\gamma\left(\max \left(x_{i}\right)-\min \left(x_{i}\right)\right) \tag{10}
\end{equation*}
$$

where $\gamma$ is a random real number between 0 and 1 . Since the Grashof condition fails, it is possible that only a small to moderate amount of individuals may survive. Therefore, during initialization it is natural to reassign $r_{1}, r_{2}, r_{3}$ and $r_{4}$ until the Grashof condition is satisfied. As pointed out by Acharyya and Mandal, the order of randomly generated $\theta_{2}^{i}(i=1-N)$ can be rearranged in CW or CCW; thereafter $\theta_{2}^{i}(i=1-N)$ are reassigned in CCW in this work.

### 3.2. Fitness

The quality of the chromosome is estimated by examining the fitness value. The fitness value is obtained by subtracting the value of the objective function as defined in Eq. (7) from a prescribed large value for the minimization problem. The prescribed large value may be chosen to avoid the fitness of a worse but feasible individual becoming negative and to maintain population diversity. The prescribed large value is 10,000 in this work. The negative fitness value is set to zero.

While the mean error is obtained, a termination criterion is then checked, as given by

$$
\begin{equation*}
e_{\mathrm{m}} \leq e_{\mathrm{tol}} \tag{11}
\end{equation*}
$$

where $e_{\text {tol }}$ is a prescribed value for error tolerance. If the termination criterion is not satisfied, the population is updated using perturbation operations to produce the next generation. The procedure is repeated until the termination criterion is satisfied or until the number of generation is equal to the prescribed number of generations $G_{\text {max }}$.

### 3.3. Selection and pairing

Roulette-wheel selection is employed in this work to allow those individuals with higher fitness to have a higher chance of being selected. Thereafter two non-repeated individuals are paired randomly to be parents.

### 3.4. Differential vector perturbations

The crossover operation in RGA is replaced by differential vector perturbation of DE, with the best individual or some excellent individuals as the base vectors. Therefore, parents are used as differential vectors, not crossover. All paired parents are randomly divided into $k$ groups corresponding to the top $k$ individuals, denoted by $\mathbf{X}_{\text {top } 1}, \mathbf{X}_{\mathrm{top} 2 \ldots} \ldots \mathbf{X}_{\mathrm{top} k}$. These form the base vectors. The value of $k$ is a user-defined integer. In the $i$-th group, the offspring may be generated by

$$
\begin{align*}
& \mathbf{X}_{1}=\mathbf{X}_{\text {topi }}+F_{1}\left(\mathbf{X}_{r 1}-\mathbf{X}_{r 2}\right)  \tag{12}\\
& \mathbf{X}_{2}=\mathbf{X}_{\text {topi }}-F_{2}\left(\mathbf{X}_{r 1}-\mathbf{X}_{r 2}\right)
\end{align*}
$$

where $\mathbf{X}_{r 1}$ and $\mathbf{X}_{r 2}$ are the parents; $F_{1}$ and $F_{2}$ are random real numbers between 0 and 1 for each design variable.
A main perturbation rate $P_{\mathrm{m} 1}$ is defined as the ratio of the expected number of offspring generated by differential vector perturbations to the total population size, while replacing crossover rate $P_{c}$ in RGA.

### 3.5. Mutation

Mutation may be useful in maintaining population diversity. Here, mutation is performed to replace randomly selected chromosome by random real numbers (that are within the limits of variables). The minor perturbation rate $P_{\mathrm{m} 2}$, i.e., mutation rate, is defined as the ratio of the expected number of offspring introduced by mutation to the total population size.

### 3.6. Elitism

The technique of elitism [28] is employed in this work is defined as follows: the best-so-far individual is always retained, replacing the current worst one, carrying on into the succeeding generation.

### 3.7. Comparison with $D E$

There are some differences between the GA-DE hybrid algorithm and DE as follows.

1. For the same number of differential vectors, the range (or the degree of uniform) of differential vector distribution for the GADE hybrid algorithm may be better than DE. This is because the definition of disturbing vectors in Eq. (12) and non-repeated individuals $\mathbf{X}_{r 1}$ and $\mathbf{X}_{r 2}$ are paired randomly. In different strategies of DE, the disturbing vector for the $\mathrm{DE} / \mathrm{x} / \mathrm{y} / \mathrm{z}$ with $y=2$ ( $x$ : object to be disturbed, $y$ : number of differential vectors, $z$ : crossover way) is obtained from 4 random individuals. However, the $\mathrm{DE} / x / 1 / z$ is the most widely used strategy, being used in the works of Cabrera et al. and Acharyya and Mandal.
2. The number of the object to be disturbed in the GA-DE hybrid algorithm can be one, two, or more, while the number of the base vector for DE is only one. This might be helpful when searching a better solution for some problems or for other purposes.
3. Both the main perturbation of the differential vectors and the minor perturbation of the mutation are used as genetic operators in the GA-DE hybrid algorithm. However, the frame of this algorithm is the same as in GA. In DE, the main perturbation of the differential vectors (called mutation in DE ) is implemented and the crossover operator is retained for population diversity.
4. The ways in which selection is carried out are parent selection and survivor selection (replacement) for the GA-DE hybrid algorithm and $D E$, respectively.

## 4. Results and discussion

The efficiency and accuracy of the proposed method are verified by studying four cases (for more than five target points) from the literature. Two sets of user-supplied parameters are used. One is for the purpose of comparison with other solutions discussed in the literature. It includes the following: size of population $N_{\mathrm{p}}=100$; only the best individual is used as the base vector for the differential vector perturbation, i.e., $k=1$; number of generations $G_{\max }=1000$ for cases $1-3$ and $G_{\max }=50$ for case 4 ; major perturbation rate $P_{\mathrm{m} 1}=0.6$; minor perturbation rate $P_{\mathrm{m} 2}=0.01$; error tolerance $e_{\mathrm{tol}}=10^{-4}$. The other is expected to help obtain more satisfactory solutions. It includes the following: size of population $N_{\mathrm{p}}=400$; top two individuals are used as the base vectors, i.e., $k=2$; the other user-supplied parameters are the same.

All the synthesized solutions in this work have been validated so that there are no circuit and order defects and they are not incapable of motion. The number $\left(N^{o}\right)$ of evaluations of the objective function and the population size are shown in the tables.

### 4.1. Case 1: 6 target points and 15 design variables

The first case is a path synthesized problem with six target points arranged in a vertical line and without prescribed timing.
Design variables: $\mathbf{X}=\left[r_{1}, r_{2}, r_{3}, r_{4}, r_{c x}, r_{c y}, x_{0}, y_{0}, \theta_{0}, \theta_{2}^{1}, \theta_{2}^{2}, \theta_{2}^{3}, \theta_{2}^{4}, \theta_{2}^{5}, \theta_{2}^{6}\right]$
Target points : $C_{d}^{i}=[(20,20),(20,25),(20,30),(20,35),(20,40),(20,45)]$
Limits of the variables : $r_{1}, r_{2}, r_{3}, r_{4} \in[5,60] ; r_{c x}, r_{c y}, x_{0}, y_{0} \in[-60,60] ; \theta_{0}, \theta_{2}^{1}, \theta_{2}^{2}, \theta_{2}^{3}, \theta_{2}^{4}, \theta_{2}^{5}, \theta_{2}^{6} \in[0,2 \pi]$.
The synthesized geometric parameters and the corresponding values of the objective function and the mean error are shown in Table 1, together with the synthesized solutions obtained by Cabrera et al. and Acharyya and Mandal. The original value of $\theta_{2}^{1}$ obtained for $N_{\mathrm{p}}=100$ and $k=1$ is 6.80719 and exceeds $2 \pi$. Therefore, its real value should be 0.524005 . Although the constraint of the sequence of the input angles during the evolution is ignored in this case, there is no order defect in the best synthesized mechanisms, as can be seen in Table 1. Obviously, the accuracy of the solution for case 1 has been remarkably improved using the present method. The mean error for $N_{\mathrm{p}}=100$ and $k=1$ obtained in this work show a decline by about $76 \%$ compared with the DE solution obtained by Acharyya and Mandal, and shows a decline by about $86 \%$ compared with the solution obtained by Cabrera et al. Clearly, the BGA solution is most unsatisfactory one. As expected, and as shown in Table 1, the solution for $N_{\mathrm{p}}=400$ and $k=2$ is more accurate than that for $N_{\mathrm{p}}=100$ and $k=1$. For $N_{\mathrm{p}}=400$ and $k=2$, we find some solutions for the objective function value on the order of $10^{-6}$. However, the order defects are encountered. Fig. 2 shows the six target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=100$ and $k=1$ for case 1 , together with that obtained by Acharyya and Mandal. Fig. 3 shows the six target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=400$ and $k=2$ for case 1 .

### 4.2. Case 2: 6 target points and 9 design variables

This case is a path synthesized problem with six target points arranged in a semi-circular arc and prescribed timing.
Design variables: $\mathbf{X}=\left[r_{1}, r_{2}, r_{3}, r_{4}, r_{c x}, r_{c y}, x_{0}, y_{0}, \theta_{0}\right]$
Target points : $C_{d}^{i}=[(0,0),(1.9098,5.8779),(6.9098,9.5106),(13.09,9.5106),(18.09,5.8779),(20,0)]$ and $\theta_{2}^{i}=\left[\frac{\pi}{6}, \frac{\pi}{3}, \frac{\pi}{2}, \frac{2 \pi}{3}, \frac{5 \pi}{6}, \pi\right]$
Limits of the variables : $r_{1}, r_{2}, r_{3}, r_{4} \in[5,50] ; r_{c x}, r_{c y}, x_{0}, y_{0} \in[-50,50] ; \theta_{0} \in[0,2 \pi]$.
The synthesized geometric parameters and the corresponding values of the objective function and the mean error are shown in Table 2, together with the synthesized solutions obtained by Acharyya and Mandal. Obviously, the BGA solution is unsound. The mean

Table 1
Synthesized results for case 1.

|  | Present |  | $[15]$ | BGA [17] <br>  <br>  <br>  <br>  <br>  <br> $N_{\mathrm{p}}=100, k=1$ |
| :--- | :--- | :--- | :--- | :--- |
| $N^{o}$ | 100,000 | $N_{\mathrm{p}}=400, k=2$ | $N_{\mathrm{p}}=100$ | $N_{\mathrm{p}}=100$ |

[^1]

Fig. 2. Six target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=100$ and $k=1$ for case 1 , together with that obtained by Acharyya and Mandal.
error for $N_{\mathrm{p}}=100$ and $k=1$ obtained in this work shows a decline by about $31 \%$ as compared with the DE solution. The improvement of the solution when $N_{\mathrm{p}}=400$ and $k=2$ is almost negligible compared to that when $N_{\mathrm{p}}=100$ and $k=1$, as shown in Table 2 . Therefore, this case should be studied further, using other algorithms or design considerations. Fig. 4 shows the six target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=100$ and $k=1$ for case 2 , together with that obtained by Acharyya and Mandal. The typical evolution of the value of the objective function of the best-so-far individual for case 2 corresponding to the number of generations, obtained with the proposed evolutionary algorithm, is shown in Fig. 5. The convergence rate for the best-so-far individual is fast. The value of the objective function of the best-so-far individual for this case almost converges to a minimum value within only 200 generations; thereafter the improvement of the objective is negligible, which is similar to the result obtained by Acharyya and Mandal.

### 4.3. Case 3: 10 target points and 19 design variables

The case is a path synthesized problem with 10 target points arranged in an ellipse and without prescribed timing.
Design variables : $\mathbf{X}=\left[r_{1}, r_{2}, r_{3}, r_{4}, r_{c x}, r_{c y}, x_{0}, y_{0}, \theta_{0}, \theta_{2}^{1}, \theta_{2}^{2}, \theta_{2}^{3}, \theta_{2}^{4}, \theta_{2}^{5}, \theta_{2}^{6}, \theta_{2}^{7}, \theta_{2}^{8}, \theta_{2}^{9}, \theta_{2}^{10}\right]$


Fig. 3. Six target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=400$ and $k=2$ for case 1 .

Table 2
Synthesized results for case 2.
$\begin{array}{lllll}\hline & \text { Present } & & \text { BGA [17] } \\$\cline { 2 - 4 } \& \(\left.\left.N_{\mathrm{p}}=100, k=1 \& N_{\mathrm{p}}=400, k=2 \& N_{\mathrm{p}}=100\end{array}\right] \begin{array}{l}DE [17] <br>

N_{\mathrm{p}}=100\end{array}\right]\)|  |
| :--- |
| $N^{o}$ |
| $r_{1}$ |



Fig. 4. Six target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=100$ and $k=1$ for case 2 , together with that obtained by Acharyya and Mandal.


Fig. 5. Typical evolution of the value of the objective function of the best-so-far individual for case 2 corresponding to the number of generations obtained with the proposed evolutionary algorithm.

Table 3
Synthesized results for case 3.

|  | Present |  | $\begin{aligned} & \text { BGA [17] } \\ & N_{\mathrm{p}}=100 \end{aligned}$ | $\begin{aligned} & \mathrm{DE}[17] \\ & N_{\mathrm{p}}=100 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: |
|  | $N_{\mathrm{p}}=100, k=1$ | $N_{\mathrm{p}}=400, k=2$ |  |  |
| $N^{o}$ | 100,000 | 400,000 | 200,000 | 100,000 |
| $r_{1}$ | 80.0 | 80.0 | 79.981513 | 54.360893 |
| $r_{2}$ | 8.24689 | 8.42032 | 9.109993 | 8.683351 |
| $r_{3}$ | 45.8968 | 51.3426 | 72.936511 | 34.318634 |
| $r_{4}$ | 58.5404 | 42.4532 | 80.0 | 79.996171 |
| $r_{c x}$ | -6.40389 | -9.3741 | 0.0 | 0.000187 |
| $r_{c y}$ | -9.12264 | 5.06098 | 0.0 | 1.46525 |
| $x_{0}$ | 6.52409 | 5.53372 | 10.155966 | 10.954397 |
| $y_{0}$ | 20.522 | 0.477183 | 10.0 | 11.074534 |
| $\theta_{0}$ | 0.136532 | 4.28177 | 0.026149 | 2.12965 |
| $\theta_{2}^{1}$ | 6.05991 | 2.0935 | 6.283185 | 6.283185 |
| $\theta_{2}^{2}$ | 0.488453 | 2.81291 | 0.600745 | 0.616731 |
| $\theta_{2}^{3}$ | 1.17805 | 3.51605 | 1.372812 | 1.310254 |
| $\theta_{2}^{4}$ | 1.88339 | 4.20638 | 2.210575 | 2.19357 |
| $\theta_{2}^{5}$ | 2.59806 | 4.89051 | 2.862639 | 2.91717 |
| $\theta_{2}^{6}$ | 3.28585 | 5.57398 | 3.420547 | 3.490746 |
| $\theta_{2}^{7}$ | 3.96674 | 6.26458 | 4.072611 | 4.132017 |
| $\theta_{2}^{8}$ | 4.65966 | 0.676189 | 4.910373 | 4.922075 |
| $\theta_{2}^{9}$ | 5.35231 | 1.38307 | 5.68244 | 5.695372 |
| $\theta_{2}^{10}$ | 6.06263 | 2.09348 | 6.283185 | 6.28297 |
| $f_{\text {obj }}$ | $3.11511 \times 10^{-2}$ | $6.02203 \times 10^{-4}$ | 5.77309 | 2542.25 |
| $e_{\mathrm{m}}$ | $4.82473 \times 10^{-2}$ | $6.74935 \times 10^{-3}$ | $7.00454 \times 10^{-1}$ | 15.8445 |

Target points : $C_{d}^{i}=\left[\begin{array}{l}(20,10),(17.66,15.142),(11.736,17.878),(5,16.928),(0.60307,12.736), \\ (0.60307,7.2638),(5,3.0718),(11.736,2.1215),(17.66,4.8577),(20,10)\end{array}\right]$
Limits of the variables : $r_{1}, r_{2}, r_{3}, r_{4} \in[5,80] ; r_{c x}, r_{c y}, x_{0}, y_{0} \in[-80,80] ; \theta_{0}, \theta_{2}^{1}, \theta_{2}^{2} \ldots \theta_{2}^{10} \in[0,2 \pi]$.
The synthesized geometric parameters and the corresponding values of the objective function and the mean error are shown in Table 3, together with the synthesized solutions obtained by Acharyya and Mandal. Although the constraint of the sequence of the input angles during the evolution is ignored in this case, there is no order defect in the best synthesized mechanisms, as can be seen in Table 3. Obviously, the DE solution is unsound. There is remarkable improvement in the accuracy of the solution for case 3 using the present method. The mean error for $N_{\mathrm{p}}=100$ and $k=1$ obtained in this work shows a decline by about $93 \%$ as compared with the BGA solution. Moreover, the BGA requires many more generations for convergence. As can be seen in Table 3, the solution for $N_{\mathrm{p}}=400$ and $k=2$ is much more accurate than that for $N_{\mathrm{p}}=100$ and $k=1$. Fig. 6 shows the ten target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=100$ and $k=1$ for case 3 , together with that obtained by Acharyya and


Fig. 6. Ten target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=100$ and $k=1$ for case 3 , together with that obtained by Acharyya and Mandal.


Fig. 7. Ten target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=400$ and $k=2$ for case 3 .

Mandal. Fig. 7 shows the ten target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=400$ and $k=2$ for case 3.

### 4.4. Case 4: 18 target points and 10 design variables

This case is a path synthesized problem with 18 target points and prescribed timing.

$$
\begin{aligned}
& \text { Design variables }: \mathbf{X}=\left[r_{1}, r_{2}, r_{3}, r_{4}, r_{c x}, r_{c y}, x_{0}, y_{0}, \theta_{0}, \theta_{2}^{1}\right] \\
& \text { Target points : } C_{d}^{i}=\left[\begin{array}{l}
(0.5,1.1),(0.4,1.1),(0.3,1.1),(0.2,1.0),(0.1,0.9),(0.005,0.75),(0.02,0.6),(0.0,0.5),(0.0,0.4), \\
(0.03,0.3),(0.1,0.25),(0.15,0.2),(0.2,0.3),(0.3,0.4),(0.4,0.5),(0.5,0.7),(0.6,0.9),(0.6,1.0)
\end{array}\right] \text { and } \theta_{2}^{i}=\left[\theta_{2}^{1}, \theta_{2}^{1}+20^{\circ} * i\right](\mathrm{i}=1,2 \ldots 17)
\end{aligned}
$$

Limits of the variables : $r_{1}, r_{2}, r_{3}, r_{4} \in[0,50] ; r_{c x}, r_{c y}, x_{0}, y_{0} \in[-50,50] ; \theta_{0} \theta_{2}^{i} \in[0,2 \pi]$.
The synthesized geometric parameters and the corresponding values of the objective function and the mean error are shown in Table 4, together with the synthesized solutions obtained by Kunjur and Krishnamurty and Cabrera et al. The mean error for $N_{\mathrm{p}}=100$ and $k=1$ increases by $14 \%$ and $34 \%$ compared to the solutions obtained by Cabrera et al. and the exact gradient method, respectively. As expected, and as shown in Table 4, the solution for $N_{\mathrm{p}}=100$ and $k=1$ has been improved by using $N_{\mathrm{p}}=400$ and $k=2$. Fig. 8 shows the eighteen target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=100$ and $k=1$ for case 4 , together with the curves obtained by Kunjur and Krishnamurty and Cabrera et al. Fig. 9 shows the eighteen target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=400$ and $k=2$ for case 4 , together with that obtained by Kunjur and Krishnamurty.

Table 4
Synthesized results for case 4.

|  | Present |  | $\begin{aligned} & {[15]} \\ & N_{\mathrm{p}}=100 \end{aligned}$ | Exact gradient[16] |
| :---: | :---: | :---: | :---: | :---: |
|  | $N_{\text {p }}=100, k=1$ | $N_{\text {p }}=400, k=2$ |  |  |
| $\mathrm{N}^{0}$ | 5000 | 400,000 | 5000 | 240 |
| $r_{1}$ | 49.9592 | 47.4379 | 3.057878 | 2.85452 |
| $r_{2}$ | 0.218612 | 0.32477 | 0.237803 | 0.36355 |
| $r_{3}$ | 42.4842 | 0.472857 | 4.828954 | 2.91374 |
| $r_{4}$ | 32.7470 | 47.3093 | 2.056456 | 0.49374 |
| $r_{c x}$ | -47.9660 | 0.118748 | 0.767038 | 1.031223 |
| $r_{c y}$ | 15.3586 | -0.319924 | 1.850828 | 1.717471 |
| $x_{0}$ | 44.1758 | 0.526988 | 1.776808 | 0.95928 |
| $y_{0}$ | -23.9643 | 0.72393 | -0.641991 | -1.19645 |
| $\theta_{0}$ | 5.37543 | 3.32029 | 1.002168 | 0.76398 |
| $\theta_{2}^{1}$ | 1.88551 | 3.51233 | 0.226186 | 0.51172 |
| $f_{\text {obj }}$ | $4.61271 \times 10^{-2}$ | $1.08613 \times 10^{-2}$ | $3.48391 \times 10^{-2}$ | $1.09034 \times 10^{-2}$ |
| $e_{\text {m }}$ | $4.78422 \times 10^{-2}$ | $2.2283 \times 10^{-2}$ | $4.21508 \times 10^{-2}$ | $2.26716 \times 10^{-2}$ |



Fig. 8. Eighteen target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=100$ and $k=1$ for case 4 , together with the curves obtained by Kunjur and Krishnamurty and Cabrera et al.

## 5. Conclusions

A GA-DE hybrid algorithm is presented to be applied to the problem of four-bar linkage synthesis. The main advantage of this evolutionary algorithm is that it is simple and easy to implement to efficiently solve complicated real-world optimization problems, with no need of deep knowledge of the searching space. The easy 2D moveable sketch method (SolidWorks®) can be used to check whether there are circuit defects or the synthesized mechanism is incapable of motion. The GA-DE hybrid algorithm is produced by combining the real-valued genetic algorithm with the differential evolution. Both the main perturbation of the differential vectors and the minor perturbation of the mutation can be used as genetic operators; the blending crossover operator might thus be unnecessary. For problems without prescribed timing, the constraint of the sequence of the input angles may be ignored by rearranging them to satisfy CW or CCW rotation during initialization and during mutation. The results for cases 1-3 show that much more accurate solutions are obtained with GA-DE hybrid algorithm than with other evolutionary methods discussed in the literature. However, this work cannot lead us to claim that the proposed evolutionary algorithm outperforms other state-of-the-art evolutionary algorithms in all possible real-world optimization problems. The conclusion we draw is that the proper combination between/among evolutionary algorithms has potential to solve the optimization problem more effectively. The present work may be extended to solve other mechanism design problems. Improvement of the proposed evolutionary algorithm might be another direction for future work.


Fig. 9. Eighteen target points and the coupler curve obtained using the proposed method with $N_{\mathrm{p}}=400$ and $k=2$ for case 4 , together with that obtained by Kunjur and Krishnamurty.

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[^0]:    * Tel.: +886 222733567 ; fax: +886 222734420 .

    E-mail address: wylin@dlit.edu.tw.

[^1]:    * The original value of $\theta_{2}^{1}$ in the final evolution is 6.80719.

