CHAPTER VECTOR MECHANICS FOR ENGINEERS: DYNAMICS

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Lecture Notes: J. Walt Oler Texas Tech University Kinematics of Rigid Bodies in Three Dimensions



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Introduction



$$\sum \vec{F} = m \vec{\bar{a}}$$
$$\sum \vec{M}_G = \dot{\vec{H}}_G$$

•The fundamental relations developed for the plane motion of rigid bodies may also be applied to the general motion of three dimensional bodies.

•The relation $\vec{H}_G = \bar{I}\vec{\omega}$ which was used to determine the angular momentum of a rigid slab is not valid for general three dimensional bodies and motion.

•The current chapter is concerned with evaluation of the angular momentum and its rate of change for three dimensional motion and application to effective forces, the impulse-momentum and the work-energy principles.

Rigid Body Angular Momentum in Three Dimensions



• Angular momentum of a body about its mass center, $\vec{H}_{\alpha} = \sum_{n=1}^{n} (\vec{r}_{1}' \times \vec{v}_{2} \land m_{1}) = \sum_{n=1}^{n} [\vec{r}_{1}' \times (\vec{\omega} \times \vec{r}_{2}') \land m_{2}]$

$$\vec{H}_G = \sum_{i=1}^{\infty} (\vec{r}_i' \times \vec{v}_i \Delta m_i) = \sum_{i=1}^{\infty} [\vec{r}_i' \times (\vec{\omega} \times \vec{r}_i') \Delta m_i]$$

• The *x* component of the angular momentum,

$$H_{x} = \sum_{i=1}^{n} \left[y_{i} \left(\vec{\omega} \times \vec{r}_{i} \right)_{z} - z_{i} \left(\vec{\omega} \times \vec{r}_{i} \right)_{y} \right] \Delta m_{i}$$

$$= \sum_{i=1}^{n} \left[y_{i} \left(\omega_{x} y_{i} - \omega_{y} x_{i} \right) - z_{i} \left(\omega_{z} x_{i} - \omega_{x} z_{i} \right) \right] \Delta m_{i}$$

$$= \omega_{x} \sum_{i=1}^{n} \left(y_{i}^{2} + z_{i}^{2} \right) \Delta m_{i} - \omega_{y} \sum_{i=1}^{n} x_{i} y_{i} \Delta m_{i} - \omega_{z} \sum_{i=1}^{n} z_{i} x_{i} \Delta m_{i}$$

$$H_{x} = \omega_{x} \int (y^{2} + z^{2}) dm - \omega_{y} \int xy \, dm - \omega_{z} \int zx \, dm$$
$$= +\bar{I}_{x} \omega_{x} - \bar{I}_{xy} \omega_{y} - \bar{I}_{xz} \omega_{z}$$
$$H_{y} = -\bar{I}_{yx} \omega_{x} + \bar{I}_{y} \omega_{y} - \bar{I}_{yz} \omega_{z}$$
$$H_{z} = -\bar{I}_{zx} \omega_{x} - \bar{I}_{zy} \omega_{y} + \bar{I}_{z} \omega_{z}$$

Rigid Body Angular Momentum in Three Dimensions



$$H_{x} = +\bar{I}_{x}\omega_{x} - \bar{I}_{xy}\omega_{y} - \bar{I}_{xz}\omega_{z}$$
$$H_{y} = -\bar{I}_{yx}\omega_{x} + \bar{I}_{y}\omega_{y} - \bar{I}_{yz}\omega_{z}$$
$$H_{z} = -\bar{I}_{zx}\omega_{x} - \bar{I}_{zy}\omega_{y} + \bar{I}_{z}\omega_{z}$$

• Transformation of $\vec{\omega}$ into \vec{H} is characterized by the inertia tensor for the body,

$$\begin{pmatrix} +\bar{I}_{x} & -\bar{I}_{xy} & -\bar{I}_{xz} \\ -\bar{I}_{yx} & +\bar{I}_{y} & -\bar{I}_{yz} \\ -\bar{I}_{zx} & -\bar{I}_{zy} & +\bar{I}_{z} \end{pmatrix}$$

• With respect to the principal axes of inertia,

$$\begin{pmatrix} \bar{I}_{x'} & 0 & 0\\ 0 & \bar{I}_{y'} & 0\\ 0 & 0 & \bar{I}_{z'} \end{pmatrix}$$
$$H_{x'} = \bar{I}_{x'} \omega_{x'} \quad H_{y'} = \bar{I}_{y'} \omega_{y'}$$

• The angular momentum $\vec{H} \, \Theta f$ a rigid body and its angular velocity have the same direction if, and only if, is directed atong a principal axis of inertia.

 $H_{z'} = \bar{I}_{z'} \omega_{z'}$

Rigid Body Angular Momentum in Three Dimensions



• The momenta of the particles of a rigid body can be reduced to:

 $\vec{L} = \text{linear momentum}$

$$= m\vec{\overline{v}}$$

 \vec{H}_G = angular momentum about G

$$H_{x} = +\bar{I}_{x}\omega_{x} - \bar{I}_{xy}\omega_{y} - \bar{I}_{xz}\omega_{z}$$
$$H_{y} = -\bar{I}_{yx}\omega_{x} + \bar{I}_{y}\omega_{y} - \bar{I}_{yz}\omega_{z}$$
$$H_{z} = -\bar{I}_{zx}\omega_{x} - \bar{I}_{zy}\omega_{y} + \bar{I}_{z}\omega_{z}$$

• The angular momentum about any other given point *O* is

$$\vec{H}_O = \vec{\bar{r}} \times m\vec{\bar{v}} + \vec{H}_G$$

Rigid Body Angular Momentum in Three Dimensions





• The angular momentum of a body constrained to rotate about a fixed point may be calculated from

 $\vec{H}_O = \vec{\bar{r}} \times m\vec{\bar{v}} + \vec{H}_G$

• Or, the angular momentum may be computed directly from the moments and products of inertia with respect to the *Oxyz* frame.

$$\vec{H}_{O} = \sum_{i=1}^{n} (\vec{r}_{i} \times \vec{v}_{i} \Delta m)$$
$$= \sum_{i=1}^{n} [\vec{r}_{i} \times (\vec{\omega} \times \vec{r}_{i}) \Delta m_{i}]$$

$$H_{x} = +I_{x}\omega_{x} - I_{xy}\omega_{y} - I_{xz}\omega_{z}$$
$$H_{y} = -I_{yx}\omega_{x} + I_{y}\omega_{y} - I_{yz}\omega_{z}$$
$$H_{z} = -I_{zx}\omega_{x} - I_{zy}\omega_{y} + I_{z}\omega_{z}$$

Principle of Impulse and Momentum



• The principle of impulse and momentum can be applied directly to the threedimensional motion of a rigid body,

*Syst Momenta*₁ + *Syst Ext Imp*₁₋₂ = *Syst Momenta*₂

- The free-body diagram equation is used to develop component and moment equations.
- For bodies rotating about a fixed point, eliminate the impulse of the reactions at *O* by writing equation for moments of momenta and impulses about *O*.

Kinetic Energy



• Kinetic energy of particles forming rigid body,

$$T = \frac{1}{2}m\overline{v}^{2} + \frac{1}{2}\sum_{i=1}^{n}\Delta m_{i}\overline{v_{i}}^{2}$$
$$= \frac{1}{2}m\overline{v}^{2} + \frac{1}{2}\sum_{i=1}^{n}\left|\vec{\omega}\times\vec{r_{i}}'\right|^{2}\Delta m_{i}$$
$$= \frac{1}{2}m\overline{v}^{2} + \frac{1}{2}(\bar{I}_{x}\omega_{x}^{2} + \bar{I}_{y}\omega_{y}^{2} + \bar{I}_{z}\omega_{z}^{2} - 2\bar{I}_{xy}\omega_{x}\omega_{y}$$
$$- 2\bar{I}_{yz}\omega_{y}\omega_{z} - 2\bar{I}_{zx}\omega_{z}\omega_{x})$$

• If the axes correspond instantaneously with the principle axes,

$$T = \frac{1}{2}m\overline{v}^2 + \frac{1}{2}(\bar{I}_{x'}\omega_{x'}^2 + \bar{I}_{y'}\omega_{y'}^2 + \bar{I}_{z'}\omega_{z'}^2)$$

• With these results, the principles of work and energy and conservation of energy may be applied to the three-dimensional motion of a rigid body.

Kinetic Energy



• Kinetic energy of a rigid body with a fixed point,

$$T = \frac{1}{2} (I_x \omega_x^2 + I_y \omega_y^2 + I_z \omega_z^2 - 2I_{xy} \omega_x \omega_y - 2I_{yz} \omega_y \omega_z - 2I_{zx} \omega_z \omega_x)$$

• If the axes *Oxyz* correspond instantaneously with the principle axes *Ox'y'z'*,

$$T = \frac{1}{2} (I_{x'} \omega_{x'}^2 + I_{y'} \omega_{y'}^2 + I_{z'} \omega_{z'}^2)$$

Sample Problem 18.1





Rectangular plate of mass m that is suspended from two wires is hit at D in a direction perpendicular to the plate.

Immediately after the impact, determine *a*) the velocity of the mass center *G*, and *b*) the angular velocity of the plate.

SOLUTION:

- Apply the principle of impulse and momentum. Since the initial momenta is zero, the system of impulses must be equivalent to the final system of momenta.
- Assume that the supporting cables remain taut such that the vertical velocity and the rotation about an axis normal to the plate is zero.
- Principle of impulse and momentum yields to two equations for linear momentum and two equations for angular momentum.
- Solve for the two horizontal components of the linear and angular velocity vectors.

Sample Problem 18.1



SOLUTION:

- Apply the principle of impulse and momentum. Since the initial momenta is zero, the system of impulses must be equivalent to the final system of momenta.
- Assume that the supporting cables remain taut such that the vertical velocity and the rotation about an axis normal to the plate is zero.

$$\vec{v} = \overline{v}_x \vec{i} + v_z \vec{k} \qquad \vec{\omega} = \omega_x \vec{i} + \omega_y \vec{j}$$

Since the *x*, *y*, and *z* axes are principal axes of inertia,

$$\vec{H}_G = \bar{I}_x \omega_x \vec{i} + \bar{I}_y \omega_y \vec{j} = \frac{1}{12} m b^2 \omega_x \vec{i} + \frac{1}{12} m a^2 \omega_y \vec{j}$$

Sample Problem 18.1



- Principle of impulse and momentum yields two equations for linear momentum and two equations for angular momentum.
- Solve for the two horizontal components of the linear and angular velocity vectors.

$$0 = mv_x - F\Delta t = m\overline{v}_z \qquad \frac{1}{2}bF\Delta t = H_x - \frac{1}{2}aF\Delta t = H_y$$
$$v_x = 0 \qquad \overline{v}_z = -F\Delta t/m \qquad = \frac{1}{12}mb^2\omega_x \qquad = \frac{1}{12}ma^2\omega_y$$
$$\overline{v} = -(F\Delta t/m)\overline{k} \qquad \omega_x = 6F\Delta t/mb \qquad \omega_y = -(6F\Delta t/ma)$$
$$\overline{\omega} = \frac{6F\Delta t}{mab}(a\overline{i} + b\overline{j})$$

Sample Problem 18.1

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 $\vec{v} - (F\Delta t/m)\vec{k}$

$$\vec{\omega} = \frac{6F\Delta t}{mab} \left(a\vec{i} + b\vec{j} \right)$$

$$\vec{H}_G = \frac{1}{12}mb^2\omega_x\vec{i} + \frac{1}{12}ma^2\omega_y\vec{j}$$

Sample Problem 18.2



A homogeneous disk of mass *m* is mounted on an axle *OG* of negligible mass. The disk rotates counter-clockwise at the rate ω_1 about *OG*.



Determine: *a*) the angular velocity of the disk, *b*) its angular momentum about O, c) its kinetic energy, and d) the vector and couple at *G* equivalent to the momenta of the particles of the disk.

SOLUTION:

- The disk rotates about the vertical axis through *O* as well as about *OG*. Combine the rotation components for the angular velocity of the disk.
- Compute the angular momentum of the disk using principle axes of inertia and noting that *O* is a fixed point.
- The kinetic energy is computed from the angular velocity and moments of inertia.
- The vector and couple at *G* are also computed from the angular velocity and moments of inertia.

Sample Problem 18.2



SOLUTION:

• The disk rotates about the vertical axis through *O* as well as about *OG*. Combine the rotation components for the angular velocity of the disk.

$$\vec{\omega} = \omega_1 \vec{i} + \omega_2 \vec{j}$$

Noting that the velocity at C is zero,

$$\vec{v}_C = \vec{\omega} \times \vec{r}_C = 0$$

$$0 = (\omega_1 \vec{i} + \omega_2 \vec{j}) \times (L\vec{i} - r\vec{j})$$

$$= (L\omega_2 - r\omega_1)\vec{k}$$

$$\omega_2 = r\omega_1/L$$

$$\vec{\omega} = \omega_1 \vec{i} - (r\omega_1/L)\vec{j}$$

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Sample Problem 18.2



$$\vec{\omega} = \omega_1 \vec{i} - (r\omega_1/L)\vec{j}$$

• Compute the angular momentum of the disk using principle axes of inertia and noting that *O* is a fixed point.

$$\vec{H}_O = I_x \omega_x \vec{i} + I_y \omega_y \vec{j} + I_z \omega_z \vec{k}$$

$$H_{x} = I_{x}\omega_{x} = \left(\frac{1}{2}mr^{2}\right)\omega_{1}$$

$$H_{y} = I_{y}\omega_{y} = \left(mL^{2} + \frac{1}{4}mr^{2}\right)\left(-r\omega_{1}/L\right)$$

$$H_{z} = I_{z}\omega_{z} = \left(mL^{2} + \frac{1}{4}mr^{2}\right)0 = 0$$

$$\vec{H}_O = \frac{1}{2}mr^2\omega_1\vec{i} - m(L^2 + \frac{1}{4}r^2)(r\omega_1/L)\vec{j}$$

• The kinetic energy is computed from the angular velocity and moments of inertia.

$$T = \frac{1}{2} \left(I_x \omega_x^2 + I_y \omega_y^2 + I_z \omega_z^2 \right) = \frac{1}{2} \left[m r^2 \omega_1^2 + m \left(L^2 + \frac{1}{4} r^2 \right) \left(-r \omega_1 / L \right)^2 \right]$$

$$T = \frac{1}{8}mr^2 \left(6 + \frac{r^2}{L^2}\right)\omega_1^2$$

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Sample Problem 18.2



 $\vec{\omega} = \omega_1 \vec{i} - (r\omega_1/L)\vec{j}$

• The vector and couple at *G* are also computed from the angular velocity and moments of inertia.

 $m\vec{v} = mr\omega_1\vec{k}$

$$\vec{H}_G = \bar{I}_{x'} \omega_x \vec{i} + \bar{I}_{y'} \omega_y \vec{j} + \bar{I}_{z'} \omega_z \vec{k}$$
$$= \frac{1}{2} m r^2 \omega_1 \vec{i} + \frac{1}{4} m r^2 (-r \omega/L) \vec{j}$$

$$\vec{H}_G = \frac{1}{2}mr^2\omega_1\left(\vec{i} - \frac{r}{2L}\vec{j}\right)$$



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Motion of a Rigid Body in Three Dimensions



 $\sum \vec{F} = m\vec{a}$ $\sum \vec{M} = \dot{\vec{H}}_G$

- Angular momentum and its rate of change are taken with respect to centroidal axes *GX*'*Y*'*Z*' of fixed orientation.
- Transformation of $\vec{\omega}$ into \vec{H} is independent of the system of coordinate axes.
- Convenient to use body fixed axes *Gxyz* where moments and products of inertia are not time dependent.
- Define rate of change of change of \vec{H} with respect to the rotating frame,

$$\dot{\vec{H}}_G\Big)_{Gxyz} = \dot{H}_x\vec{i} + \dot{H}_y\vec{j} + \dot{H}_z\vec{k}$$

Then,

$$\dot{\vec{H}}_G = \left(\dot{\vec{H}}_G\right)_{Gxyz} + \vec{\Omega} \times \vec{H}_G \qquad \qquad \vec{\Omega} = \vec{\omega}$$

Euler's Eqs of Motion & D'Alembert's Principle



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$$\sum \vec{M}_G = \left(\dot{\vec{H}}_G \right)_{Gxyz} + \vec{\Omega} \times \vec{H}_G$$

Euler's Equations:

$$\sum M_{x} = \bar{I}_{x}\dot{\omega}_{x} - (\bar{I}_{y} - \bar{I}_{z})\omega_{y}\omega_{z}$$

$$\sum M_{y} = \bar{I}_{y}\dot{\omega}_{y} - (\bar{I}_{z} - \bar{I}_{x})\omega_{z}\omega_{x}$$

$$\sum M_{z} = \bar{I}_{z}\dot{\omega}_{z} - (\bar{I}_{x} - \bar{I}_{y})\omega_{x}\omega_{y}$$

- System of external forces and effective forces are equivalent for general three dimensional motion.
- System of external forces are equivalent to the vector and couple, $m\vec{a}$ and \vec{H}_G .

Motion About a Fixed Point or a Fixed Axis



- For a rigid body rotation around a fixed point, $\sum \vec{M}_{O} = \vec{H}_{O}$ $= \left(\dot{\vec{H}}_{O} \right)_{Oxyz} + \vec{\Omega} \times \vec{H}_{O}$
- For a rigid body rotation around a fixed axis, $H_x = -I_{xz}\omega$ $H_y = -I_{yz}\omega$ $H_z = -I_z\omega$

$$\begin{split} \Sigma \vec{M}_{O} &= \left(\dot{\vec{H}}_{O} \right)_{Oxyz} + \vec{\omega} \times \vec{H}_{O} \\ &= \left(-I_{xz} \vec{i} - I_{yz} \vec{j} + I_{z} \vec{k} \right) \dot{\omega} \\ &+ \omega \vec{k} \times \left(-I_{xz} \vec{i} - I_{yz} \vec{j} + I_{z} \vec{k} \right) \omega \\ &= \left(-I_{xz} \vec{i} - I_{yz} \vec{j} + I_{z} \vec{k} \right) \alpha + \left(-I_{xz} \vec{j} + I_{yz} \vec{i} \right) \omega^{2} \end{split}$$

$$\sum M_{x} = -I_{xz}\alpha + I_{yz}\omega^{2}$$
$$\sum M_{y} = -I_{yz}\alpha + I_{xz}\omega^{2}$$
$$\sum M_{z} = I_{z}\alpha$$

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Rotation About a Fixed Axis



- For a rigid body rotation around a fixed axis, $\sum M_x = -I_{xz}\alpha + I_{yz}\omega^2$ $\sum M_y = -I_{yz}\alpha + I_{xz}\omega^2$ $\sum M_z = I_z\alpha$
- If symmetrical with respect to the xy plane, $\sum M_x = 0 \quad \sum M_y = 0 \quad \sum M_z = I_z \alpha$
- If not symmetrical, the sum of external moments will not be zero, even if $\alpha = 0$,

$$\sum M_x = I_{yz}\omega^2 \quad \sum M_y = I_{xz}\omega^2 \quad \sum M_z = 0$$

• A rotating shaft requires both static $(\omega = 0)$ and dynamic $(\omega \neq 0)$ balancing to avoid excessive vibration and bearing reactions.

Sample Problem 18.3





Rod *AB* with weight W = 20 kg is pinned at *A* to a vertical axle which rotates with constant angular velocity ω = 15 rad/s. The rod position is maintained by a horizontal wire *BC*.

Determine the tension in the wire and the reaction at *A*.

SOLUTION:

- Evaluate the system of effective forces by reducing them to a vector at mached at G and couple \vec{H}_G .
- Expressing that the system of external forces is equivalent to the system of effective forces, write vector expressions for the sum of moments about *A* and the summation of forces.
- Solve for the wire tension and the reactions at *A*.

Sample Problem 18.3



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SOLUTION:

• Evaluate the system of effective forces by reducing them to a vector attraccent hed at G and couple \vec{H}_G .

$$\vec{a} = \vec{a}_n = -r\omega^2 \vec{I} = -\left(\frac{1}{2}L\cos\beta\right)\omega^2 \vec{I}$$
$$= -\left(135\,\mathrm{m/s^2}\right)\vec{I}$$

 $m\vec{a} = (20 \text{ kg})(-135 \text{ m/s}^2) = -(2700 \text{ N})\vec{I}$

$$\vec{H}_{G} = \bar{I}_{x}\omega_{x}\vec{i} + \bar{I}_{y}\omega_{y}\vec{j} + \bar{I}_{z}\omega_{z}\vec{k}$$

$$\bar{I}_{x} = \frac{1}{2}mL^{2} \qquad \bar{I}_{y} = 0 \qquad \bar{I}_{z} = \frac{1}{2}mL^{2}$$

$$\omega_{x} = -\omega\cos\beta \qquad \omega_{y} = \omega\sin\beta \qquad \omega_{z} = 0$$

$$\vec{H}_{G} = -\frac{1}{12}mL^{2}\omega\cos\beta\vec{i}$$

$$\vec{H}_{G} = (\vec{H}_{G})_{Gxyz} + \vec{\omega} \times \vec{H}_{G}$$

$$= 0 + (-\omega\cos\beta\vec{i} + \omega\sin\beta\vec{j}) \times (\frac{1}{12}mL^{2}\omega\cos\beta\vec{i})$$

$$= \frac{1}{12}mL^{2}\omega^{2}\sin\beta\cos\beta\vec{k} = (935\,\mathrm{N}\cdot\mathrm{m})\vec{k}$$

Sample Problem 18.3



• Expressing that the system of external forces is equivalent to the system of effective forces, write vector expressions for the sum of moments about *A* and the summation of forces.

$$\begin{split} \Sigma \vec{M}_A &= \Sigma \left(\vec{M}_A \right)_{eff} \\ 2.08 \vec{J} \times \left(-T \vec{I} \right) + 0.6 \vec{I} \times \left(-196 \vec{J} \right) = 1.04 \vec{J} \times \left(-2700 \vec{I} \right) + 935 \vec{K} \\ & (2.08T - 118) \vec{K} = (2808 + 935) \vec{K} \\ & T = 1856 \,\text{N} \end{split}$$

$$\begin{split} \Sigma \vec{F} &= \sum \left(\vec{F} \right)_{eff} \\ A_X \vec{I} + A_Y \vec{J} + A_Z \vec{K} - 1856 \vec{I} - 196 \vec{J} = -2700 \vec{I} \\ & \vec{A} = -(844 \,\text{N}) \vec{I} + (196 \,\text{N}) \vec{J} \end{split}$$

Motion of a Gyroscope. Eulerian Angles



•A gyroscope consists of a rotor with its mass center fixed in space but which can spin freely about its geometric axis and assume any orientation.

- From a reference position with gimbals and a reference diameter of the rotor aligned, the gyroscope may be brought to any orientation through a succession of three steps:
 - 1) rotation of outer gimbal through φ about AA',
 - 2) rotation of inner gimbal through θ about *BB*',
 - 3) rotation of the rotor through ψ about *CC*'.
- φ , θ , and ψ are called the *Eulerian Angles* and
 - $\dot{\phi}$ = rate of precession
 - $\dot{\theta}$ = rate of nutation
 - $\dot{\Psi}$ = rate of spin

Motion of a Gyroscope. Eulerian Angles



• The angular velocity of the gyroscope, $\vec{\omega} = \dot{\phi}\vec{K} + \dot{\theta}\vec{j} + \dot{\Psi}\vec{k}$

with
$$\vec{K} = -\sin\theta \vec{i} + \cos\theta \vec{j}$$

 $\vec{\omega} = -\dot{\phi}\sin\theta \vec{i} + \dot{\theta}\vec{j} + (\dot{\Psi} + \dot{\phi}\cos\theta)\vec{k}$

• Equation of motion,

$$\sum \vec{M}_{O} = \left(\dot{\vec{H}}_{O}\right)_{Oxyz} + \vec{\Omega} \times \vec{H}_{O}$$
$$\vec{H}_{O} = -I'\dot{\phi}\sin\theta\vec{i} + I'\dot{\theta}\vec{j} + I\left(\dot{\Psi} + \dot{\phi}\cos\theta\right)\vec{k}$$
$$\vec{\Omega} = \dot{\phi}\vec{K} + \dot{\theta}\vec{j}$$

 $\sum M_x = -I'(\ddot{\phi}\sin\theta + 2\dot{\theta}\dot{\phi}\cos\theta) + I\dot{\theta}(\dot{\Psi} + \dot{\phi}\cos\theta)$ $\sum M_y = I'(\ddot{\theta} - \dot{\phi}^2\sin\theta\cos\theta) + I\dot{\phi}\sin\theta(\dot{\Psi} + \dot{\phi}\cos\theta)$ $\sum M_z = I\frac{d}{dt}(\dot{\Psi} + \dot{\phi}\cos\theta)$

Steady Precession of a Gyroscope







Steady precession, $\theta, \dot{\phi}, \dot{\psi}$ are constant

 $\vec{\omega} = -\dot{\phi}\sin\theta\,\vec{i} + \omega_z\vec{k}$ $\vec{H}_O = -I'\dot{\phi}\sin\theta\,\vec{i} + I\omega_z\vec{k}$ $\vec{\Omega} = -\dot{\phi}\sin\theta\,\vec{i} + \dot{\phi}\cos\theta\,\vec{k}$

 $\sum \vec{M}_{O} = \vec{\Omega} \times \vec{H}_{O}$ $= (I\omega_{z} - I'\dot{\phi}\cos\theta)\dot{\phi}\sin\theta\vec{j}$

Couple is applied about an axis perpendicular to the precession and spin axes When the precession and spin axis are at a right angle,

$$\theta = 90^{\circ}$$
$$\sum \vec{M}_{O} = I \dot{\Psi} \dot{\phi} \vec{j}$$

Gyroscope will precess about an axis perpendicular to both the spin axis and couple axis.

Motion of an Axisymmetrical Body Under No Force



- Consider motion about its mass center of an axisymmetrical body under no force but its own weight, e.g., projectiles, satellites, and space craft. $\vec{H}_G = 0$ $\vec{H}_G = \text{constant}$
- Define the Z axis to be aligned with \vec{H} and z in a rotating axes system along the axis of symmetry. The x axis is chosen to lie in the Zz plane.

$$H_{x} = -H_{G} \sin \theta = I' \omega_{x} \qquad \qquad \omega_{x} = -\frac{H_{G} \sin \theta}{I'}$$
$$H_{y} = 0 = I' \omega_{y} \qquad \qquad \omega_{y} = 0$$
$$H_{z} = H_{G} \cos \theta = I \omega_{z} \qquad \qquad \omega_{z} = \frac{H_{G} \cos \theta}{I}$$

• θ = constant and body is in steady precession.

• Note:
$$-\frac{\omega_x}{\omega_z} = \tan \gamma = \frac{I}{I'} \tan \theta$$

Motion of an Axisymmetrical Body Under No Force



Two cases of motion of an axisymmetrical body which under no force which involve no precession:

• Body set to spin about its axis of symmetry,

 $\omega_x = H_x = 0$ $\vec{\omega}$ and \vec{H}_G are aligned

and body keeps spinning about its axis of symmetry.

• Body is set to spin about its transverse axis,

 $\omega_z = H_z = 0$ $\vec{\omega}$ and \vec{H}_G are aligned

and body keeps spinning about the given transverse axis.

Motion of an Axisymmetrical Body Under No Force



The motion of a body about a fixed point (or its mass center) can be represented by the motion of a body cone rolling on a space cone. In the case of steady precession the two cones are circular.

- I < I'. Case of an elongated body. $\gamma < \theta$ and the vector ω lies inside the angle *ZGz*. The space cone and body cone are tangent externally; the spin and precession are both counterclockwise from the positive *z* axis. The precession is said to be *direct*.
- I > I'. Case of a flattened body. $\gamma > \theta$ and the vector ω lies outside the angle ZGz. The space cone is inside the body cone; the spin and precession have opposite senses. The precession is said to be *retrograde*.