

# Emulsion Processing - Homogenization -



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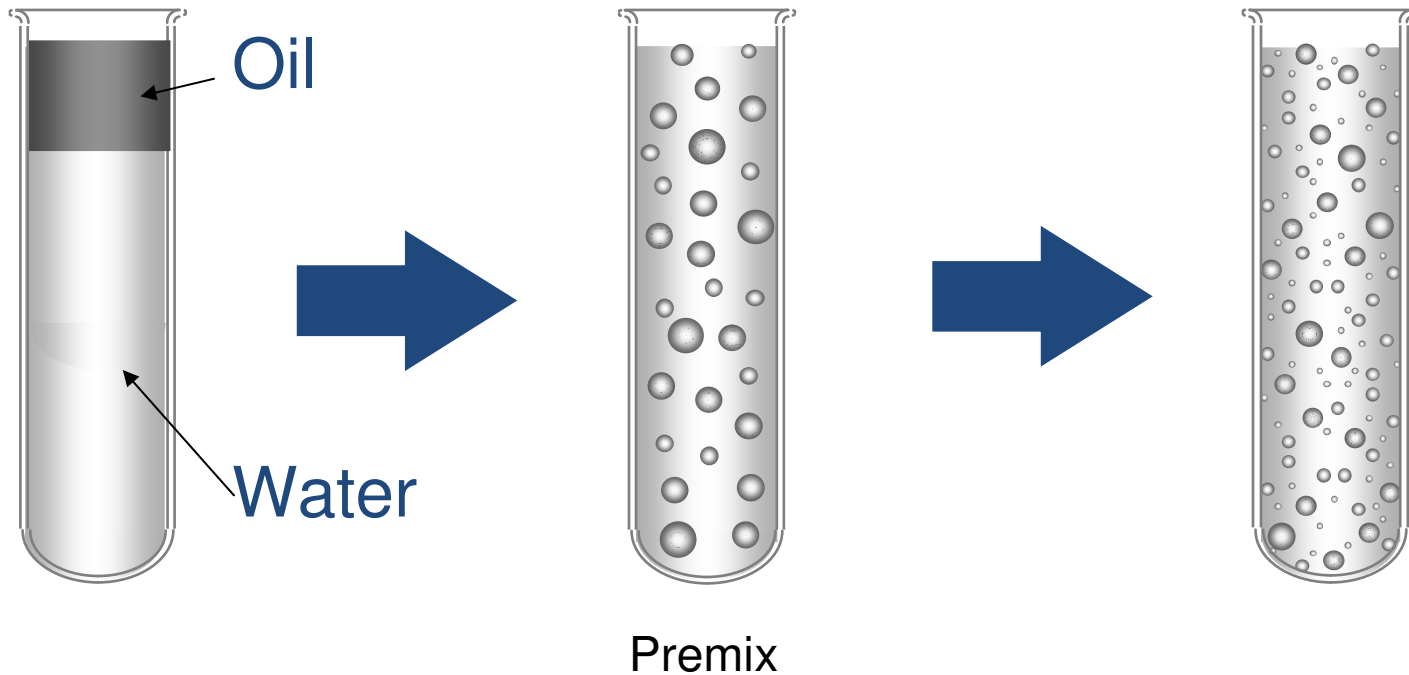
Emulsion Workshop

November 13-14<sup>th</sup>, 2008, Amherst, MA

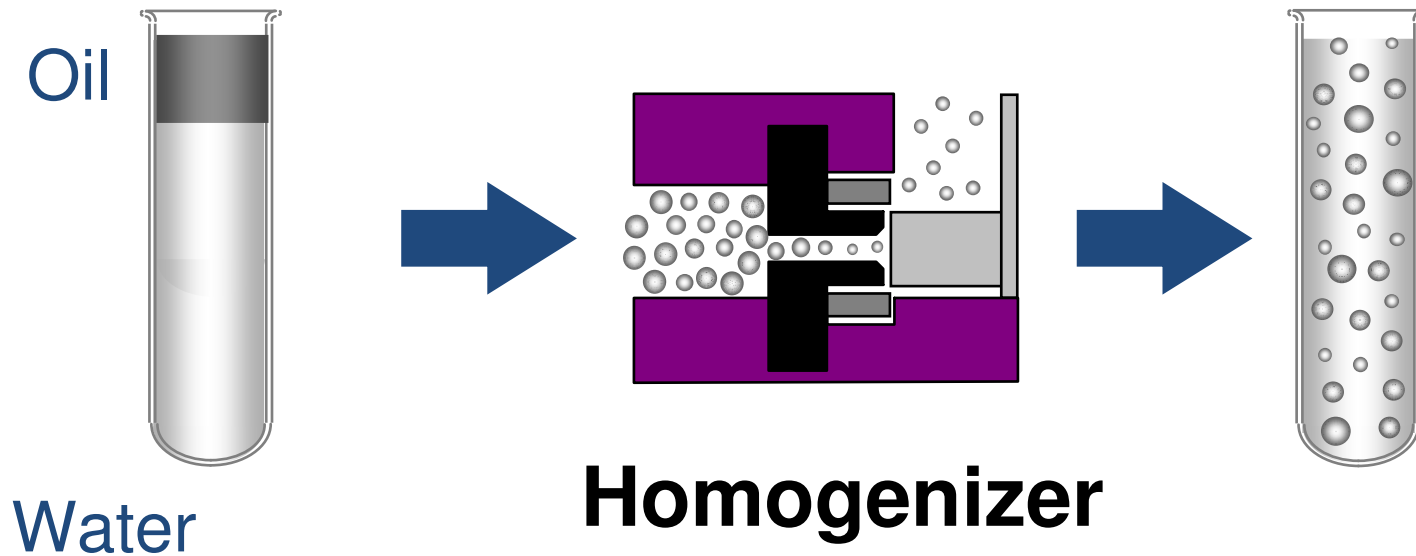
# Principle of Emulsion Formation

**Primary  
Homogenization**

**Secondary  
Homogenization**

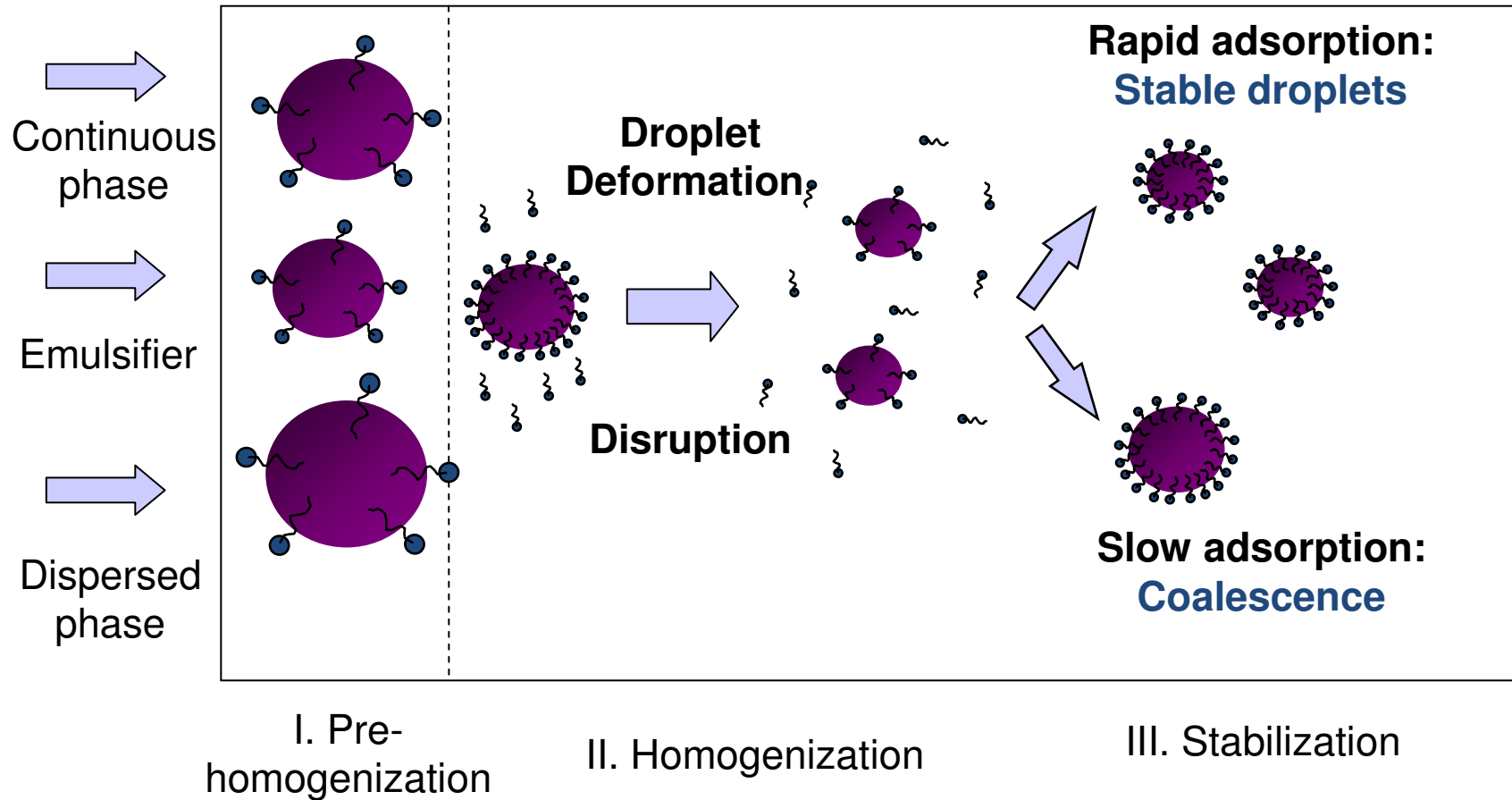


# Emulsion Processing: Homogenizers

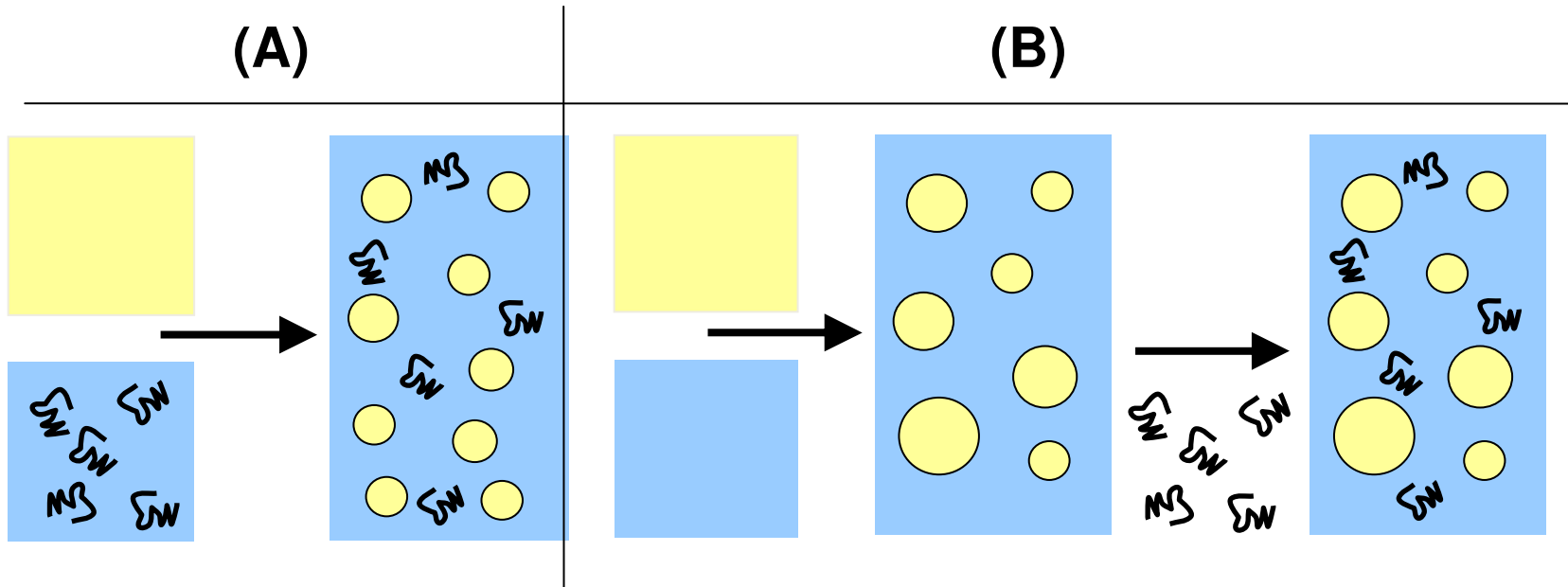


Homogenization is a unit operation using a class of processing equipment referred to as *homogenizers* that are geared towards reducing the size of droplets in liquid-liquid dispersions

# Physiochemical Processes Occurring During Homogenization



# General Homogenization Options



The order of ingredient addition and homogenization may have a large impact on product properties

# Homogenization: Process Parameters

## ■ Energy density

- minimum droplet size achievable

## ■ Energy efficiency

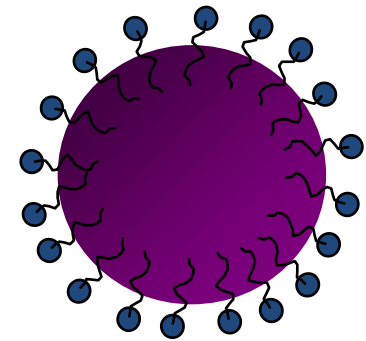
- heat losses - manufacturing costs

## ■ Volume Flow Rates

- throughput - production time

## ■ Product rheology

- limitations - materials that can be homogenized



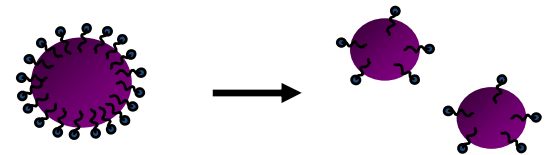
# The Physics of Droplet Disruption

- **Maintaining Force.** Drop shape maintenance forces (Laplace Pressure)
- **Disruptive Force.** Drop disruption is due to drop-surface applied tangential stresses
- **Weber-Number (We):** The ratio between drop disrupting and drop maintaining forces, drop disruption occurs only above a critical Weber number
  - $We < We_{crit}$  or  $t_{br} < t_{br,crit} \rightarrow$  droplet deformation
  - $We > We_{crit}$  or  $t_{br} > t_{br,crit} \rightarrow$  droplet disruption
- **Deformation Time.** Droplets must be exposed to tangential stresses for a sufficient amount of time

$$p_c = \gamma \left( \frac{1}{r_1} + \frac{1}{r_2} \right) = \gamma \frac{4}{d}$$

$$We = \frac{\tau}{p_c} = \frac{\tau d}{4\gamma}$$

$$t_{br,crit} = \frac{\eta_d}{\tau - p_c}$$



# Key Parameter: Energy Density $E_v$

$$E_v = \frac{\text{Energy input } E}{\text{homogenized volume } V} = \frac{P}{\dot{V}} = P_v t_v$$

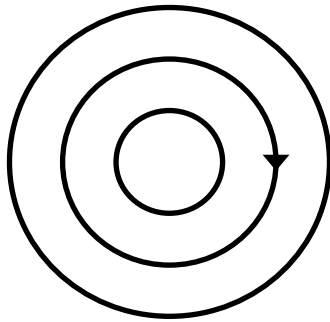
- The volume specific energy input or the energy density  $E_v$  can simply be calculated from the power consumption and the volume flow rate
- The mean droplet diameter may often be empirically related to the energy density,  $IF$ , all other parameters are kept constant!

$$x_{1,2} = C (E_v)^b$$

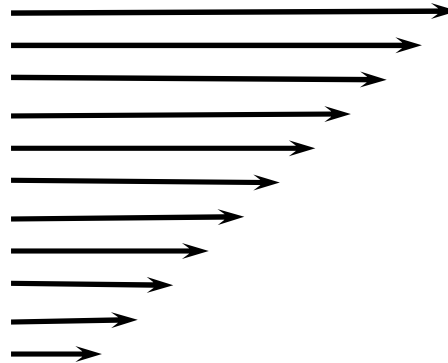


# How Droplets Are Disrupted: Flow Situations in Homogenizers

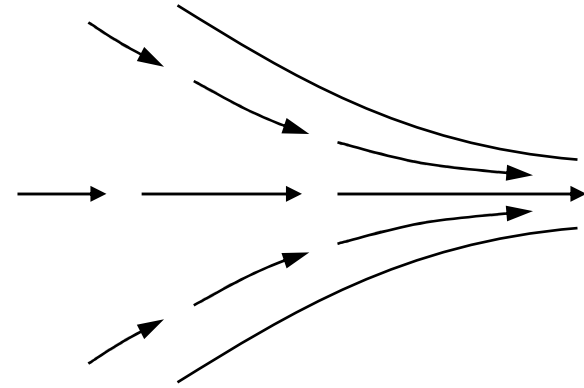
Rotational  
Flow



Simple Shear  
Flow

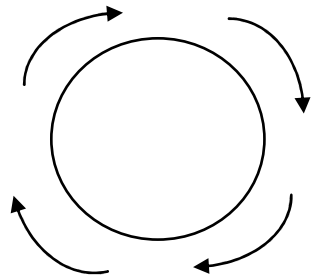


Elongational  
Flow

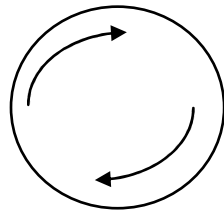


- Flow profiles are complex based on geometry of homogenizer.
- Flow may be laminar (rotational, simple shear, elongation) or turbulent.

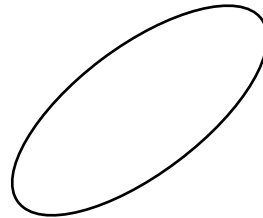
# Simple Deformation Scenarios For Liquid-Liquid Dispersions



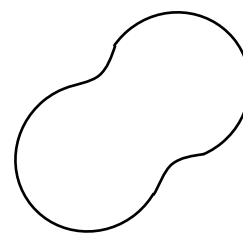
Rotation of whole droplet



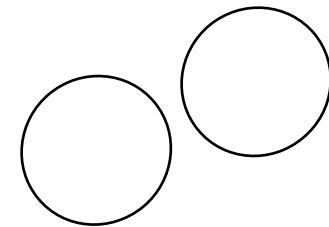
Circulation of fluid within droplet



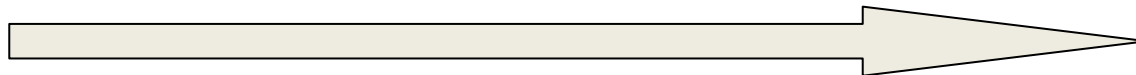
Elongation of droplet



“Neck” Formation



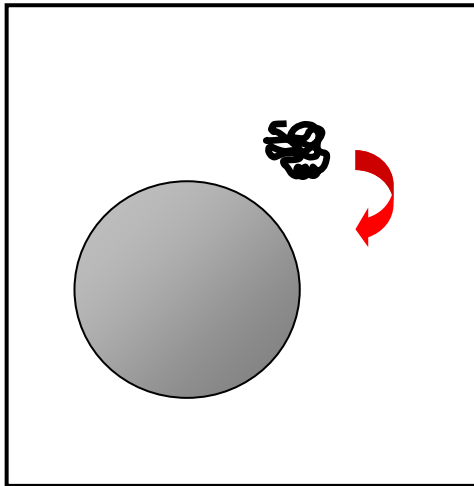
Disruption of droplet



**Increased Exertion of Stress Due to Superimposed Flow Profile**

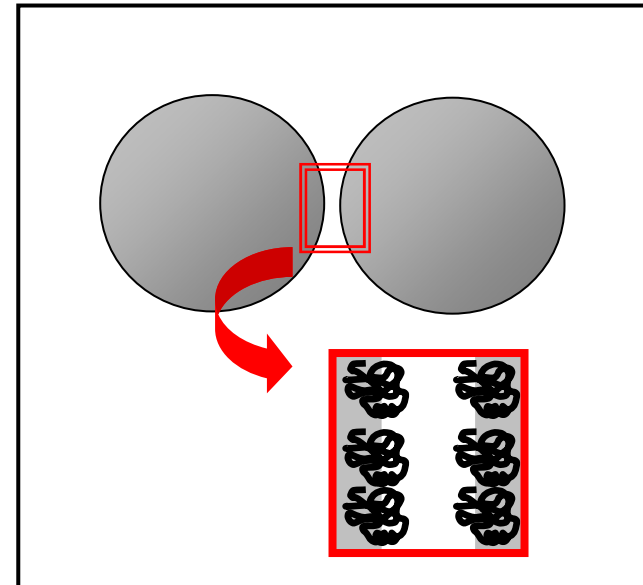
# Role of Emulsifiers in Emulsion Formation and Stabilization

## Formation



- Rapidly adsorb
- Lower interfacial tension
- Facilitate breakup

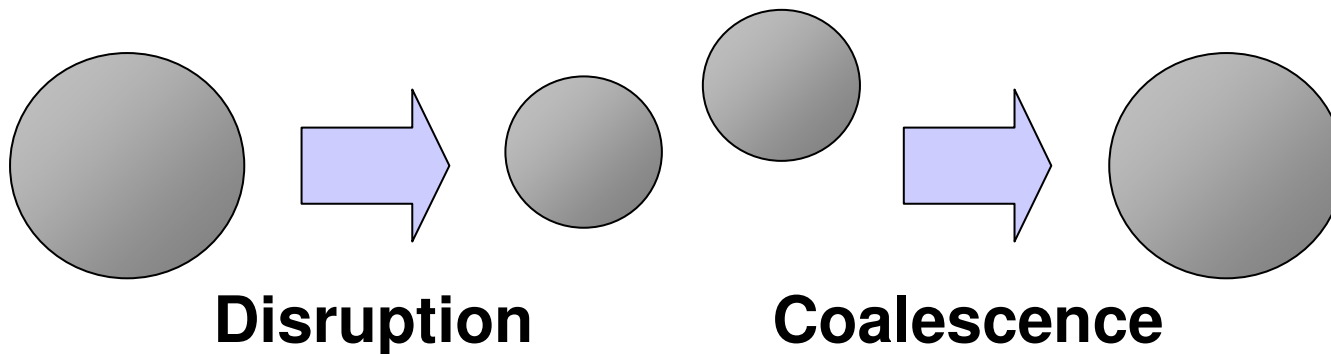
## Stabilization



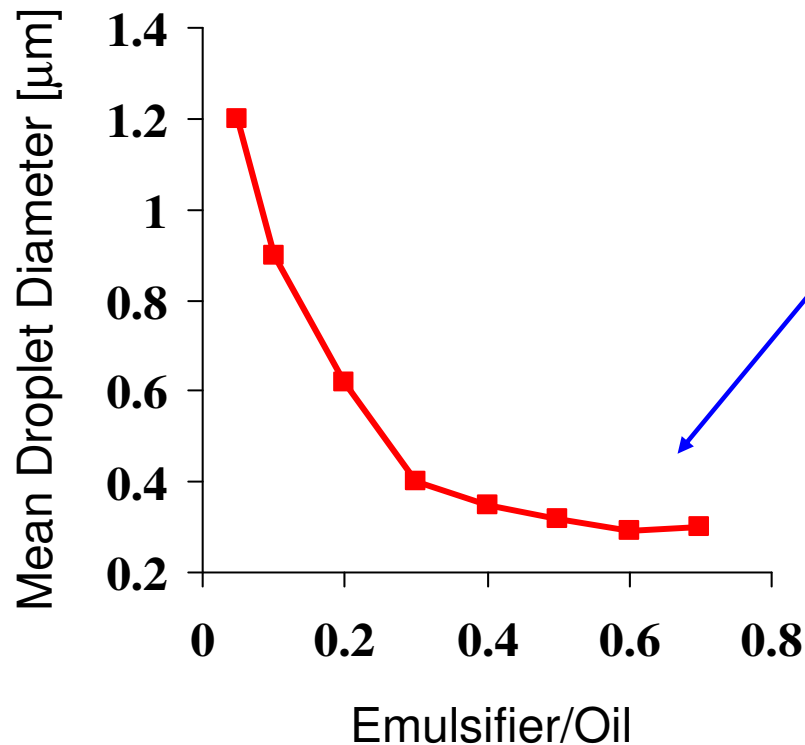
- Generate repulsive forces
- Form resistant membrane
- Prevent Coalescence

# Optimum Emulsifier Characteristics for Emulsion Formation

- **Objective:** to generate small stable droplets
  - Rapid adsorption
  - Lower interfacial Tension
  - Form protective membrane



# Factors Affecting Droplet Size: Emulsifier Concentration

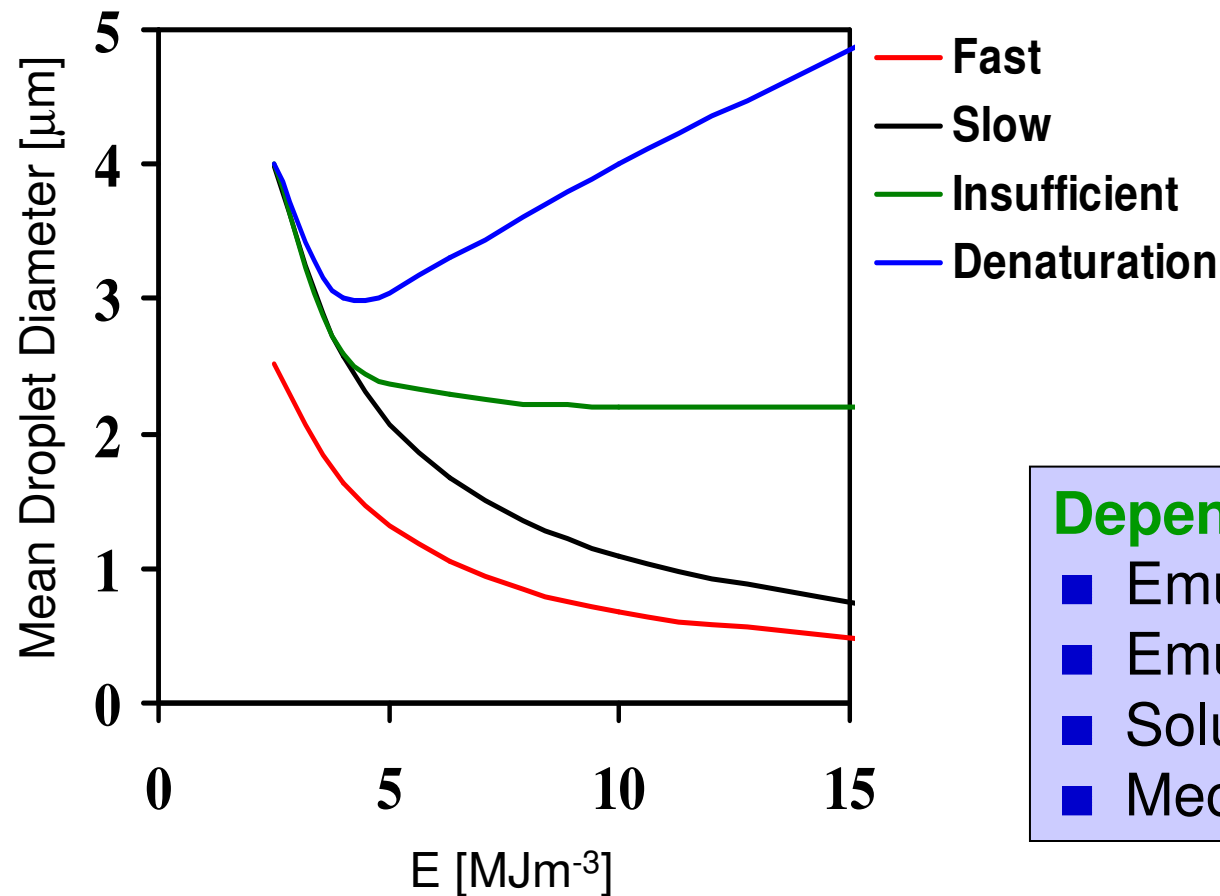


Once the emulsifier concentration exceeds a certain level the droplet size depends on the energy input of the homogenizer.

Fixed Homogenization Conditions (1000 psi)

Corn O/W emulsion - Pandolfe (1995)

# Factors Affecting Droplet Size: Emulsifier Type



## Depends on:

- Emulsifier Type
- Emulsifier Conc.
- Solution Conditions
- Mechanical Device

# Characterizing Emulsifier Efficiency During Homogenization

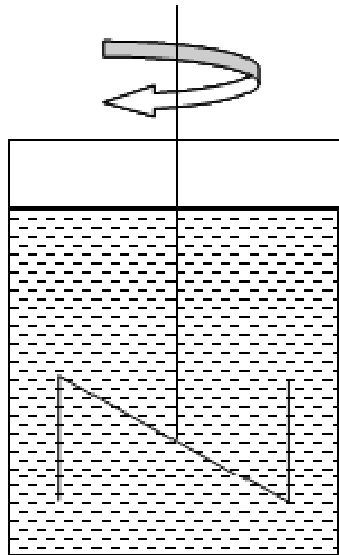
- Maximum amount of oil that can be homogenized by fixed amount of emulsifier using standardized conditions (homogenization, pH, I, T)
  - EAI (g oil / g emulsifier) – Emulsifier activity index
- Minimum amount of emulsifier required to achieve a given droplet size using standardized conditions ( $\phi$ , homogenization, pH, I, T)
  - $c_{\min}$  (g emulsifier / g oil)
- Minimum droplet size that can be achieved by homogenization
  - $r_{\min}$  ( $\mu\text{m}$ )

# Homogenizers

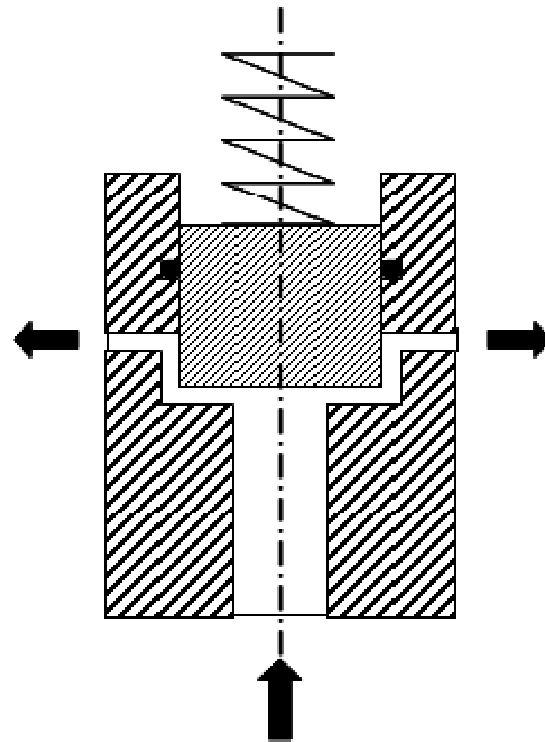
High Speed Blender  
High Pressure Homogenizers  
Colloid Mill  
High Shear Dispersers  
Ultrasonic Disruptor  
Membrane Homogenizers



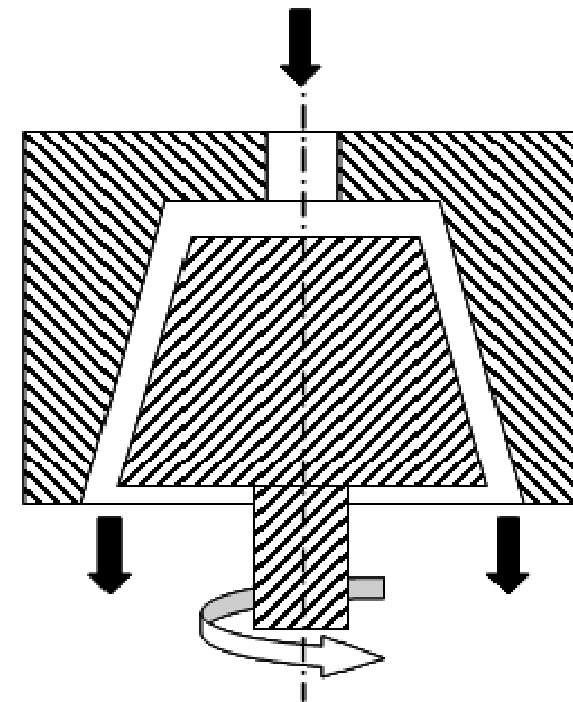
# Homogenizers: A General Overview (I)



**Rotor-Stator  
Systems  
(Blenders)**

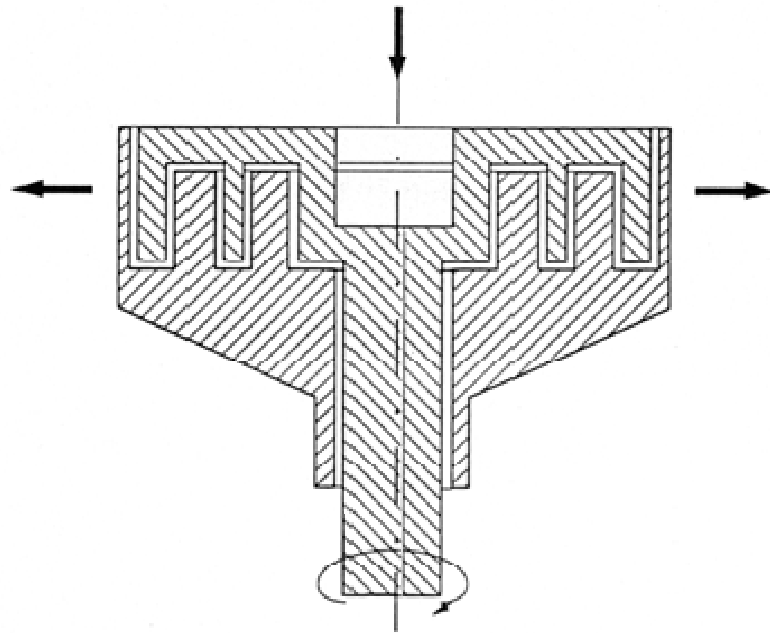


**High-Pressure  
Homogenizers /  
Microfluidizer**



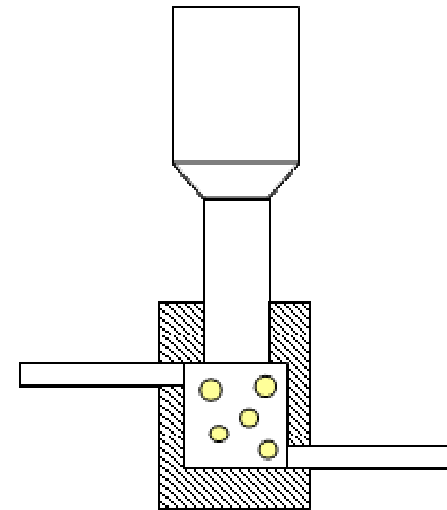
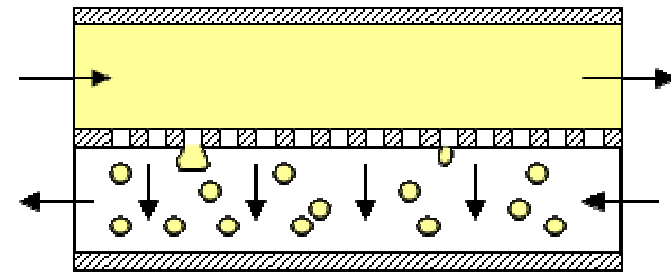
**Colloid Mill**

# Homogenizers: A General Overview (II)



**High Shear Dispenser  
(Turrax)**

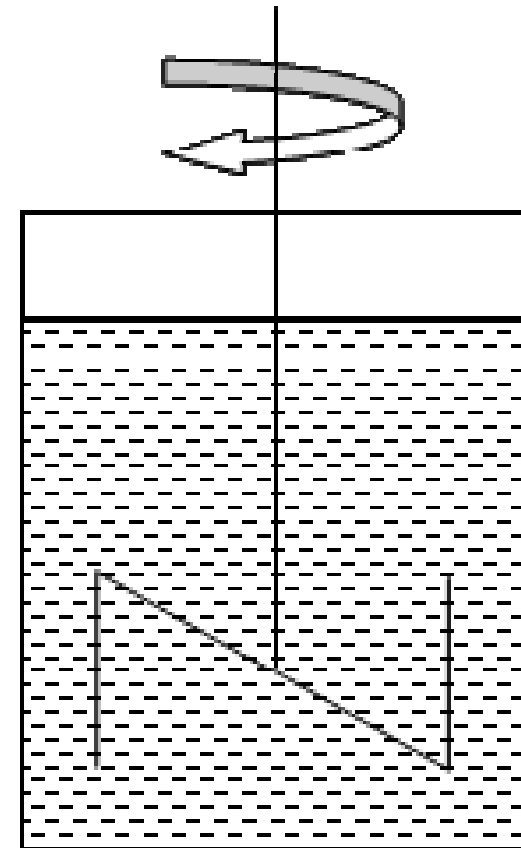
## Membrane Homogenizer



**Ultrasonicator**

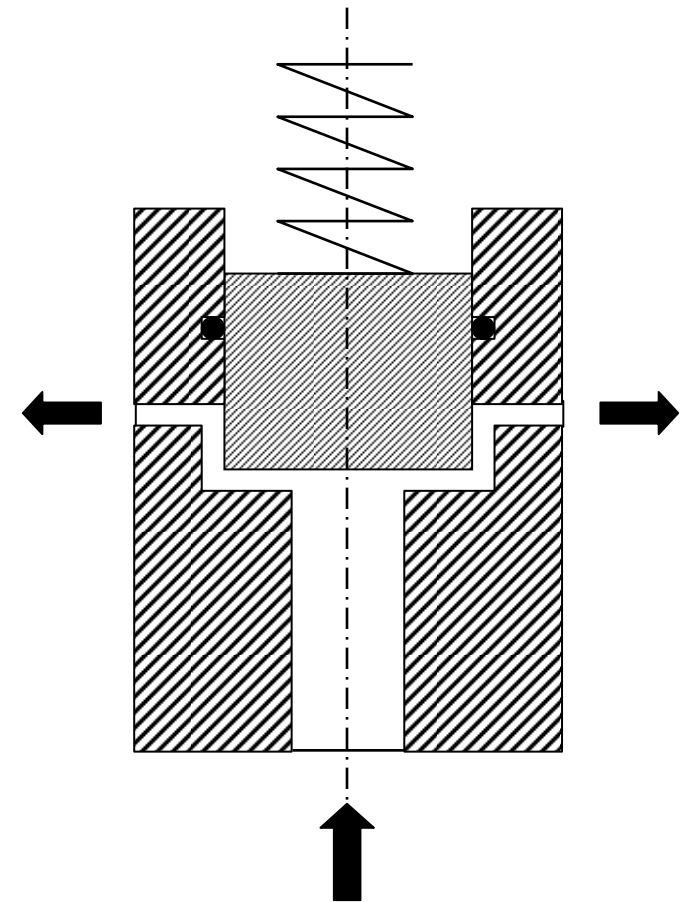
# I. High Speed Blenders

- Low volume specific energy input (energy density)
- Energy input highly distributed in the stirred vessel (regions of low and high shear)
- Blender geometry and rotational speed are the prime parameters → turbulent flows preferred.
- Broad particle size distribution, large particles
- Need to avoid air incorporation to avoid foam formation
- Fairly inexpensive usually used for premix production



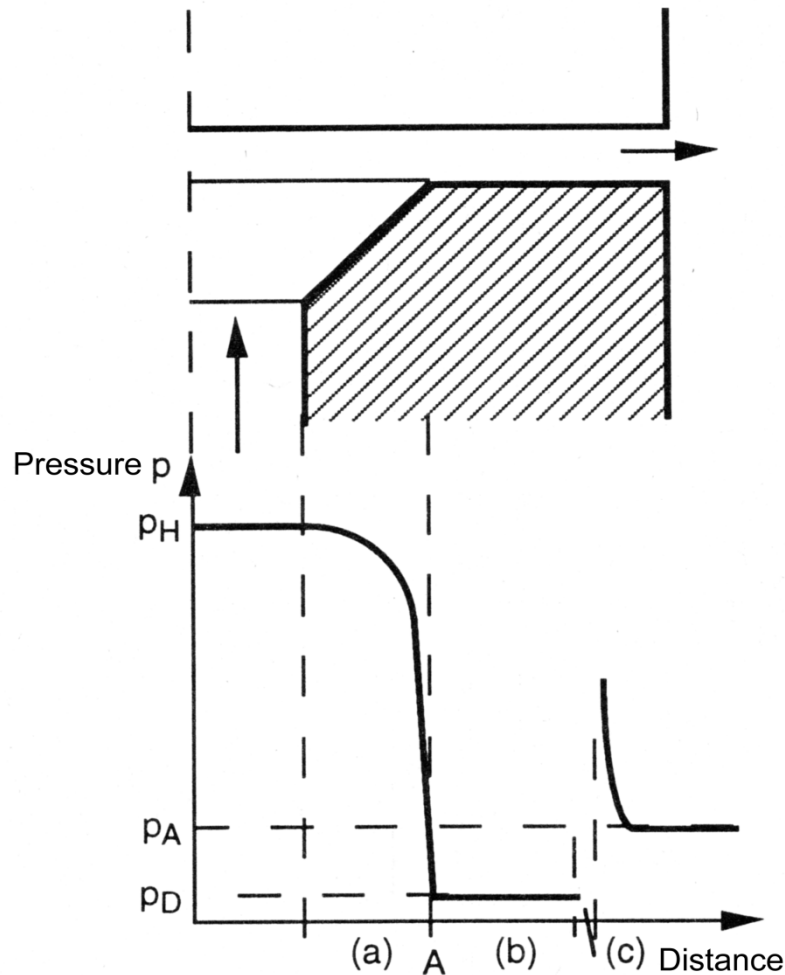
## II. High Pressure Homogenizer (HPH)

- Most common used homogenizer in the food industry (milk, cream etc.)
- Disruptive energy comes from relaxation of high pressure build up across homogenization valve
- Pressures typically range from 50 to 500 bar (microfluidizer up to 1600 bar)
- Homogenization valve geometry of key importance → influences flow profile
- Homogenization may be single or multiple stage



**Shear, Turbulent &  
Cavitation Forces**

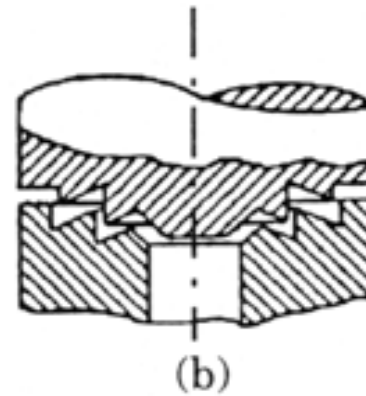
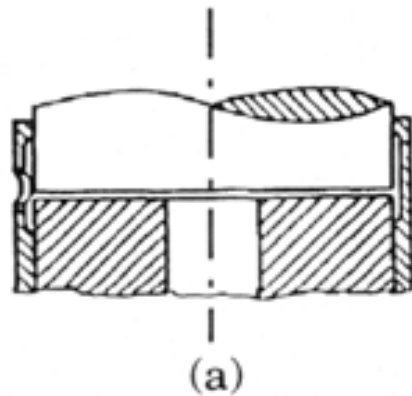
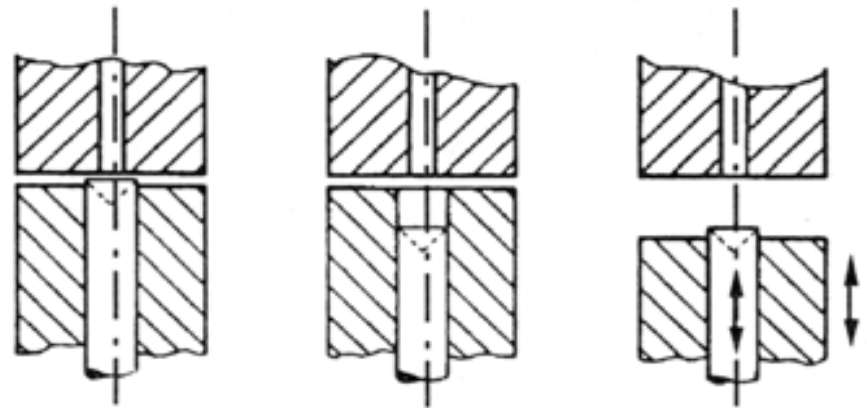
# Physical Process Inside the Homogenization Valve



- On entering the homogenization valve, the flow speed greatly increases  $\rightarrow$  pressure drops (Bernoulli) to reach the vapor pressure  $p_D$  at point A
- Since  $p_D$  is lower than the external pressure  $p_A \rightarrow$  cavitation and two phase fluid flow
- Pressure signal transduction in multi-phase flows is slower than in single phase flow  $\rightarrow$  equilibration with external pressure occurs late (close to exit)
- Sudden pressure jump leads to collapse of cavitation bubbles and the flow reverts to a one-phase flow
- Droplet disruption is therefore due to
  - Laminar and turbulent flow at entrance of valve (a)
  - Growth of cavitation bubbles in zone (b)
  - Collapse of bubbles in zone (c)

# High Pressure Homogenizer: Efficiency Requirements

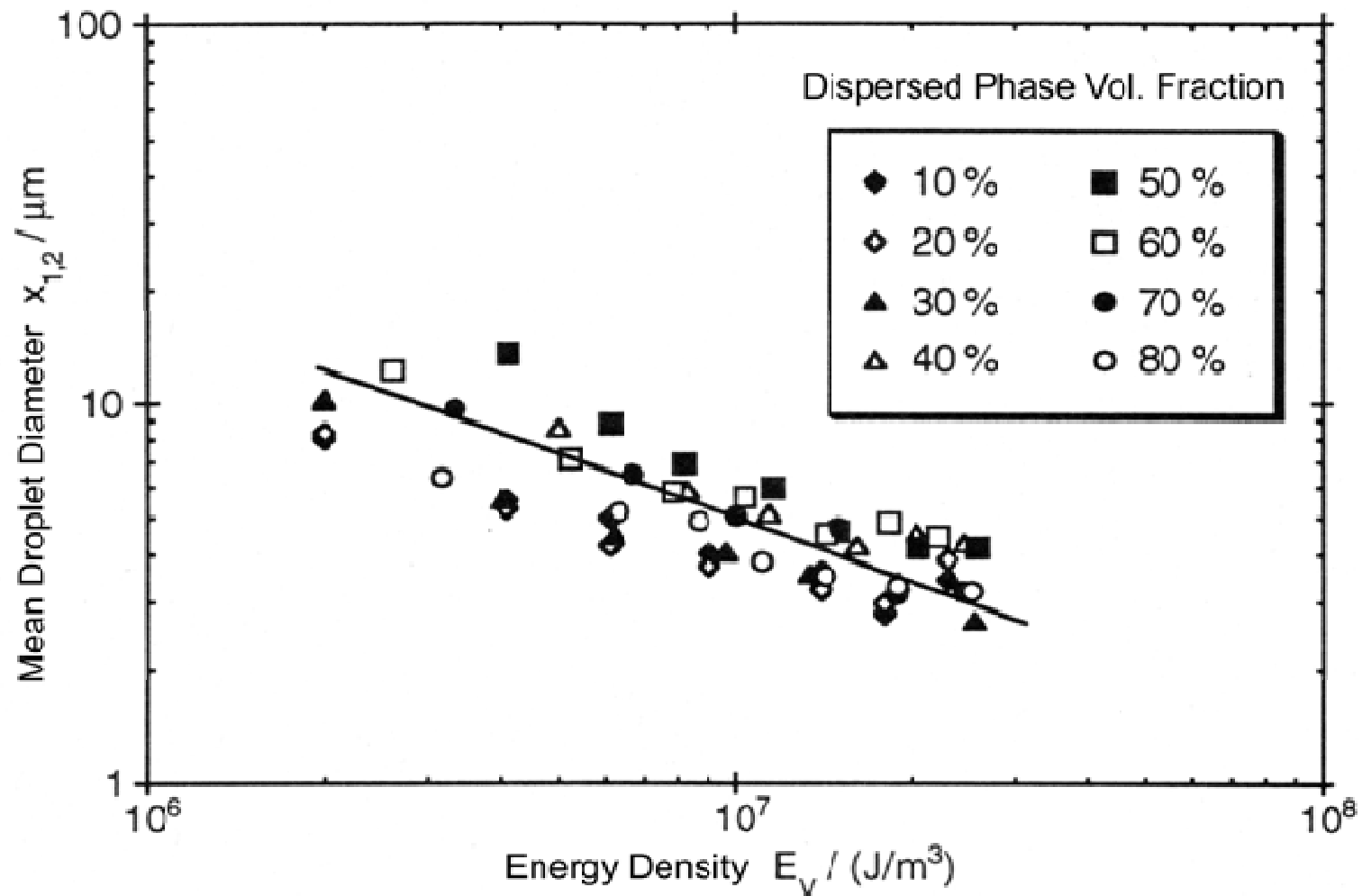
- Valve Type
  - Flat, toothed or knife edge
- Homogenization Pressure
  - Gap Size
- Counter Pressure



# HPH Efficiency Requirements

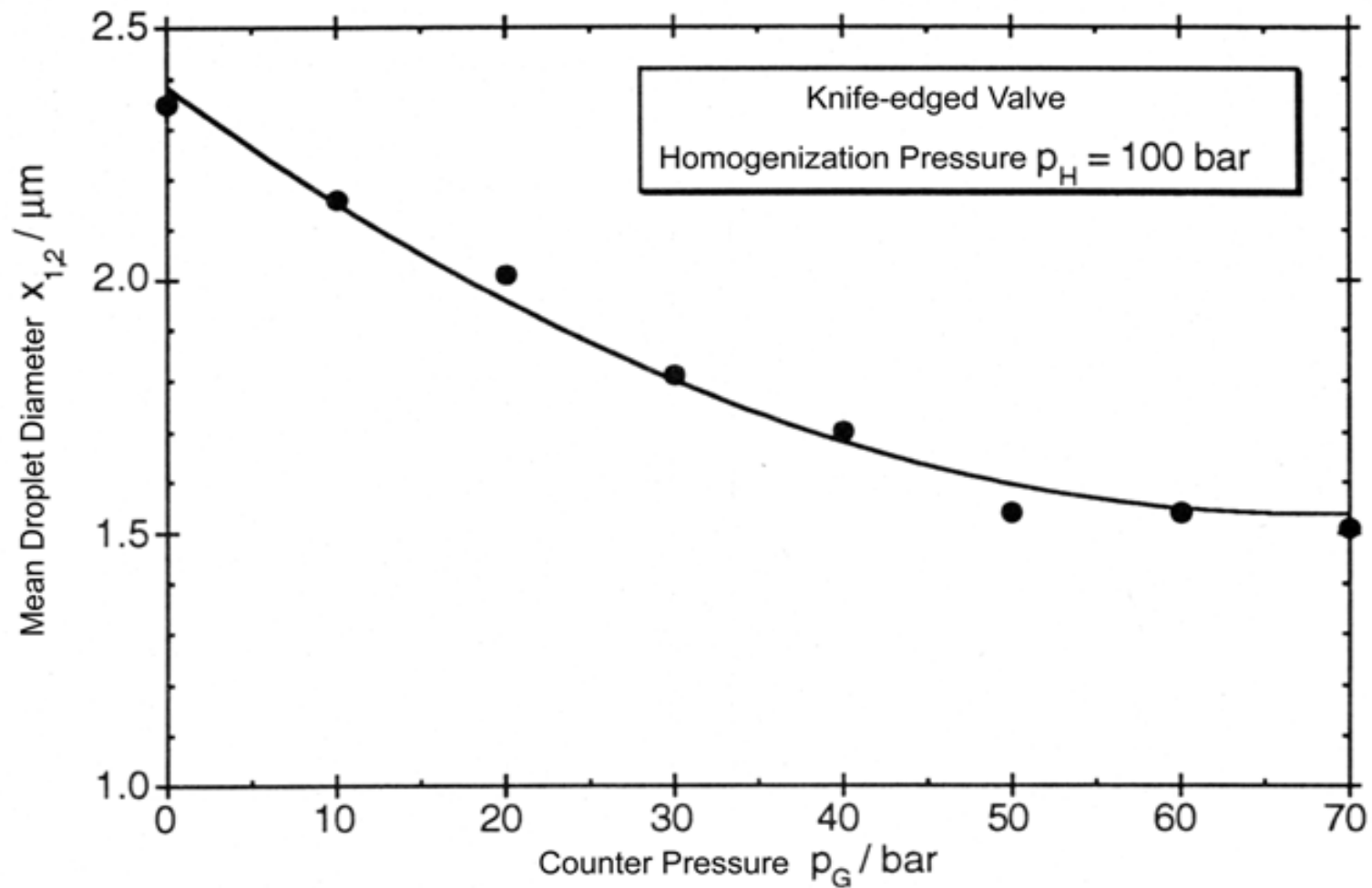
- Homogenization valves are therefore designed with the following criteria in mind
  - Ensure sufficient time for growth of cavitation bubbles
  - “Explosive” increase of pressure towards the exit
  - Maximum height of the “Dirac-like” pressure increase
- Base process parameters for the user are homogenization pressure  $p_H$  and external (exit) pressure  $p_A$
- The exit pressure may be increased through
  - Increased pressure in connected process equipment
  - Introduction of secondary pressure valve
  - Introduction of secondary homogenization valve

# HPH: Influence of Homogenization Pressure (Energy Density)

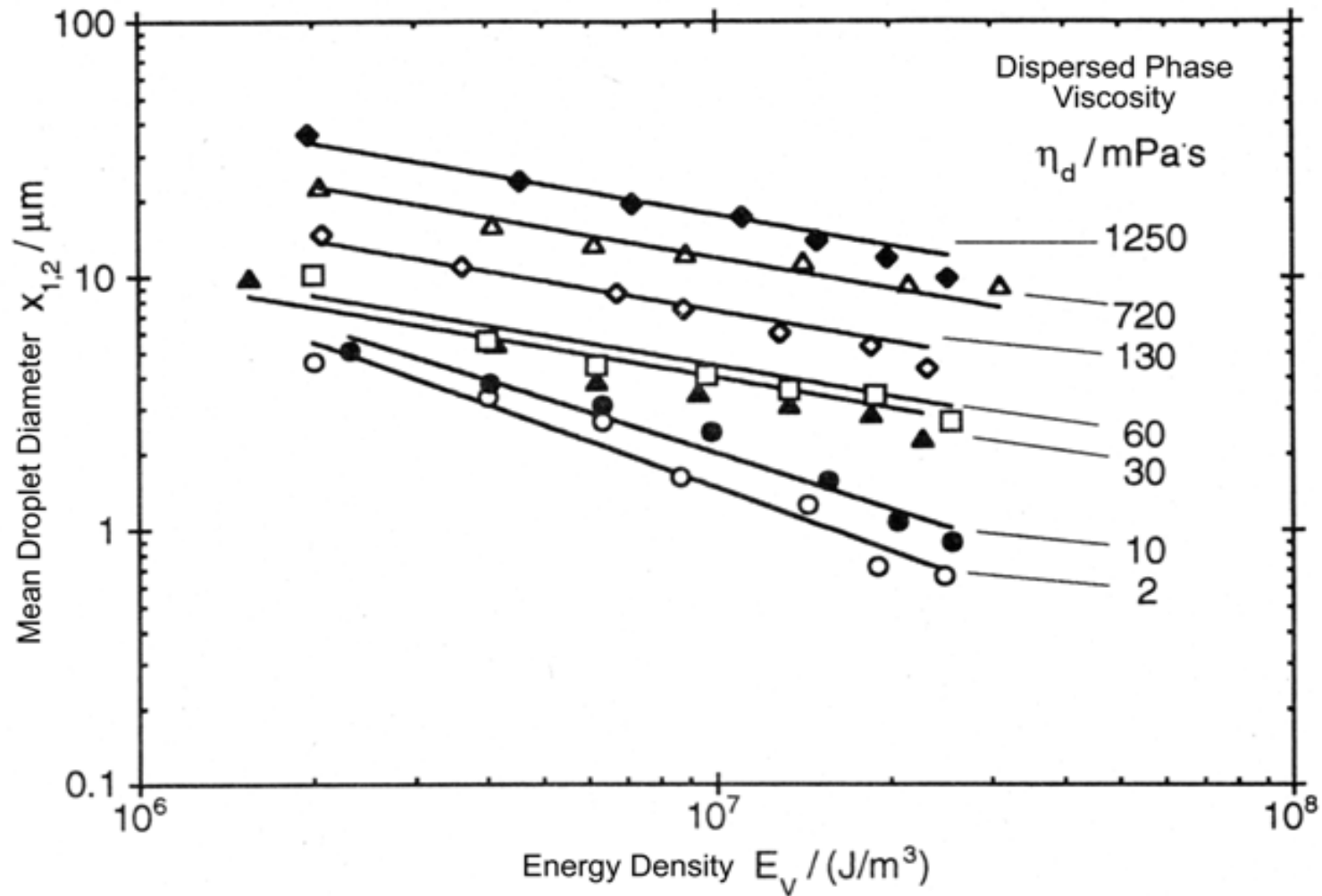




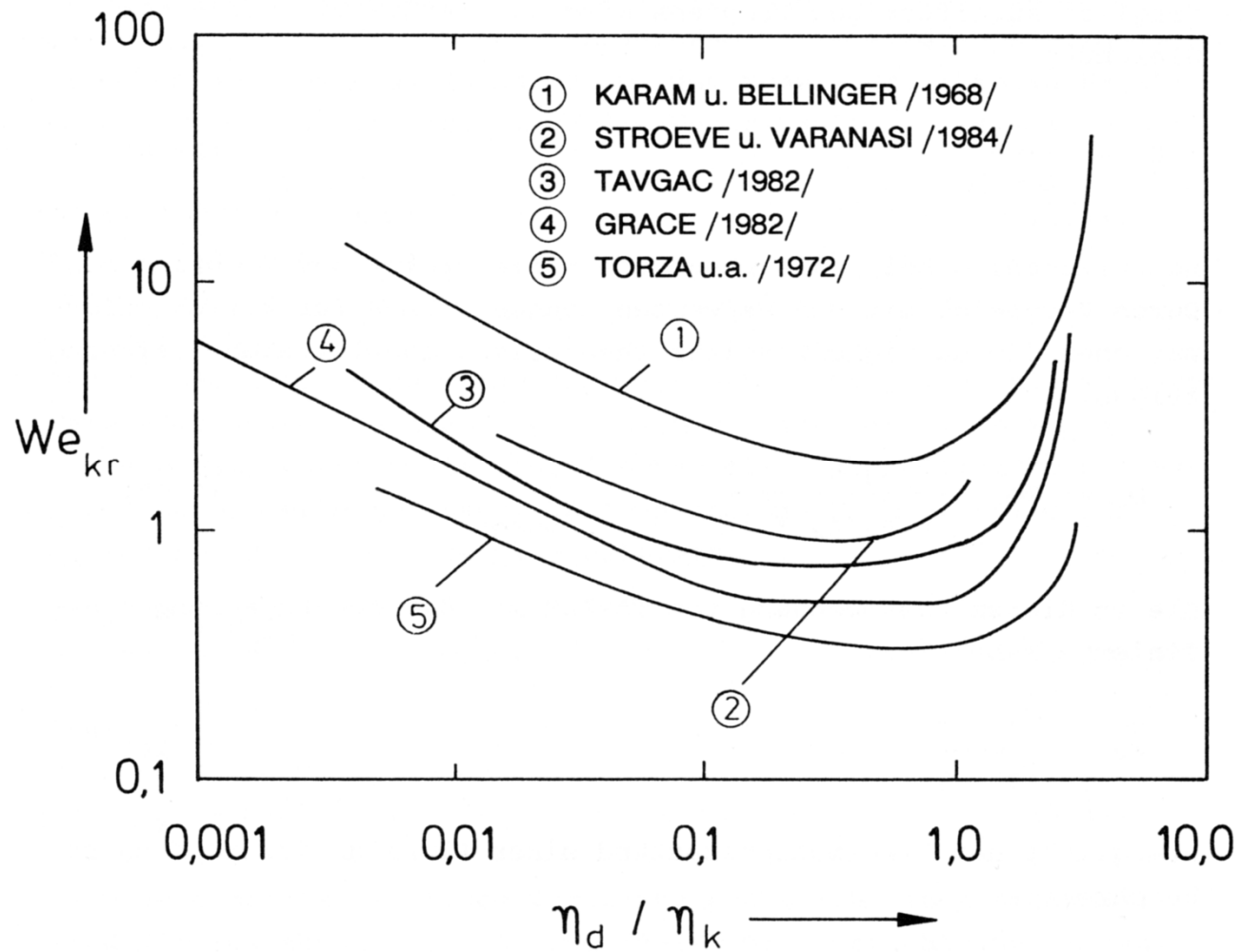
# HPH: Influence of Counter Pressure



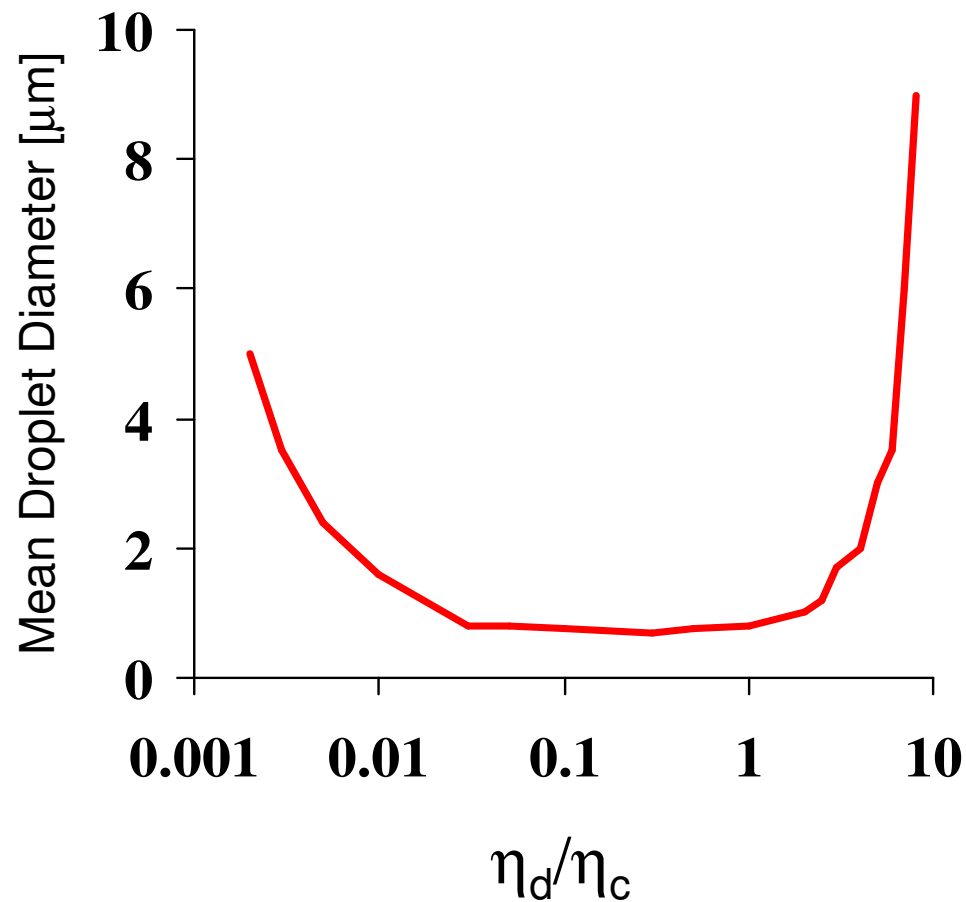
# High Pressure Homogenizer: Influence of Dispersed Phase Viscosity



# High Pressure Homogenizer: Influence of Viscosity Ratio



# Influence of Disperse and Continuous Phase Viscosity

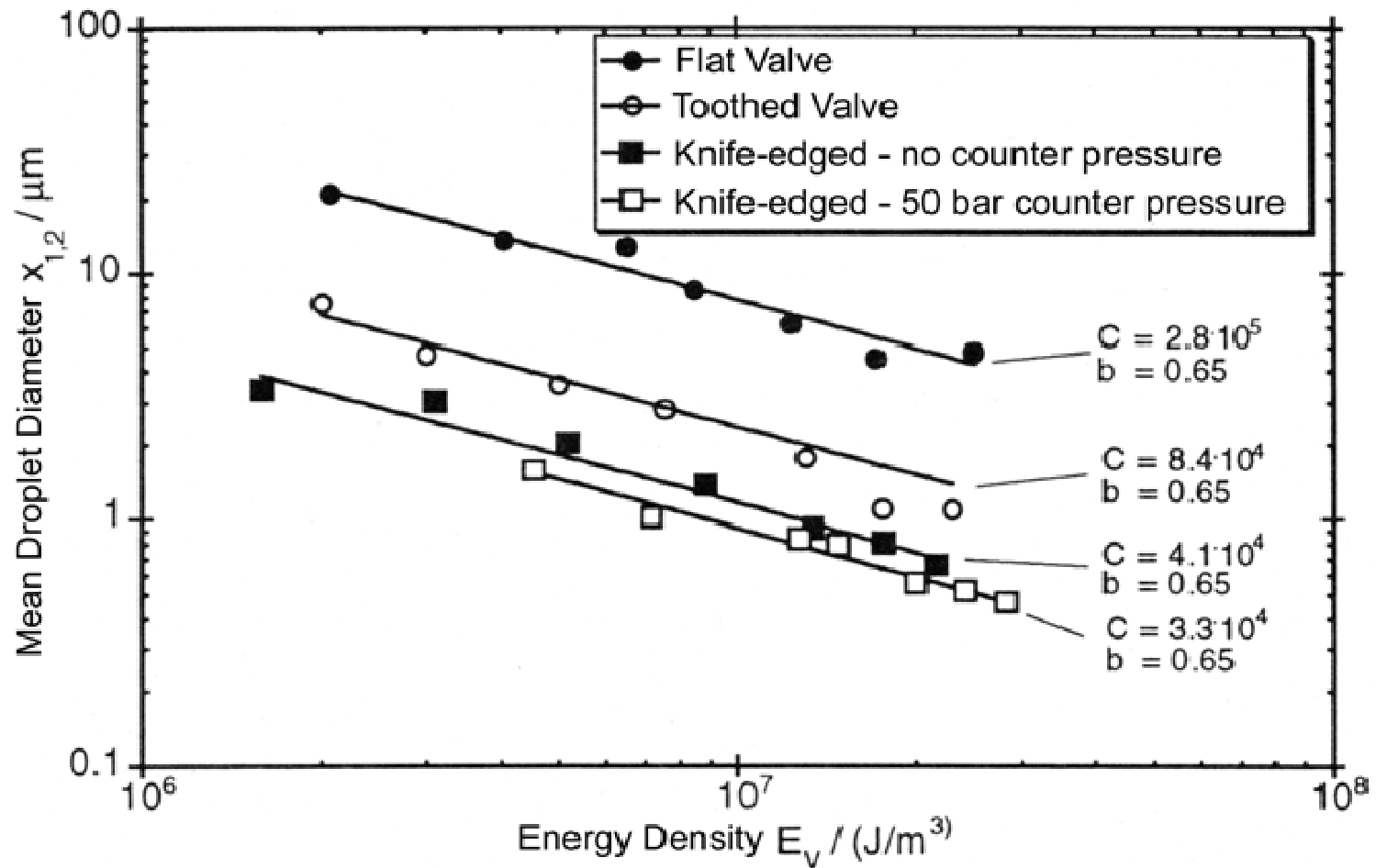


## Viscosity Ratio:

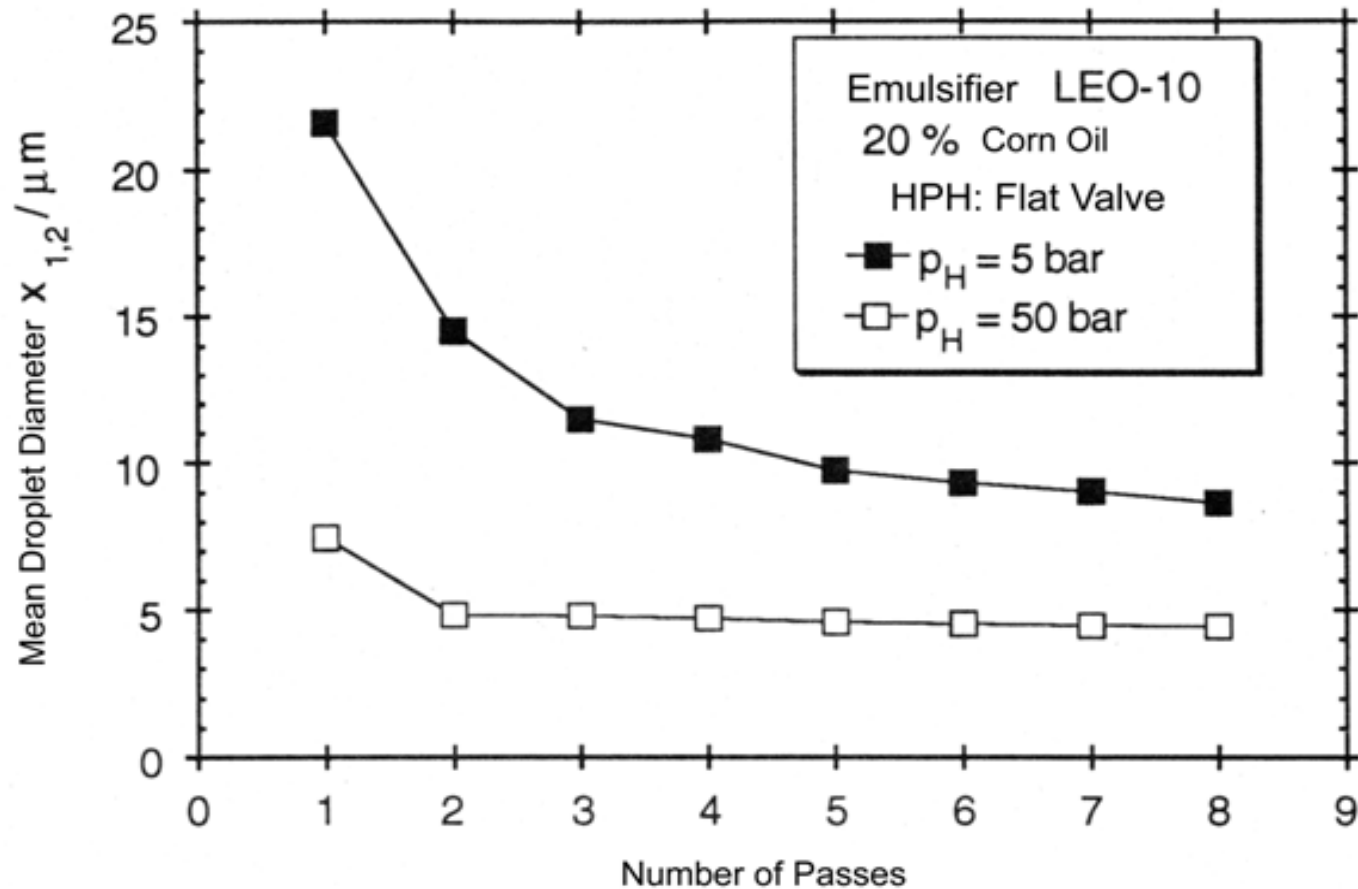
Small droplets can only be formed when viscosity ratio of oil to aqueous phase is between 0.05 and 5. It is therefore important to control viscosity ratio.

Laminar Flow Conditions, O/W Emulsions, Fast Emulsifier  
(Schubert and Armbruster, 1992)

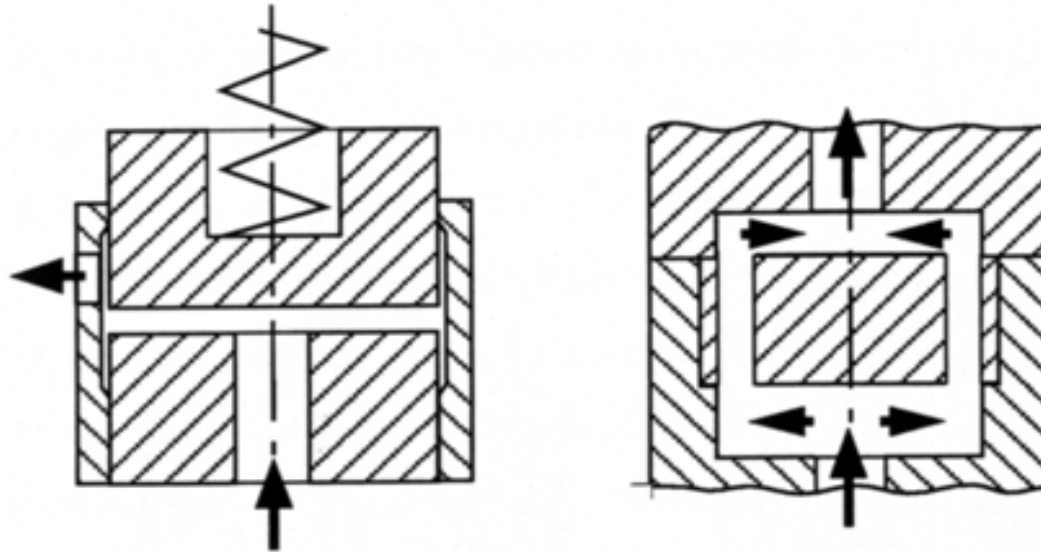
# HPH: Influence of Valve Geometry



# HDH: Multistep Homogenization

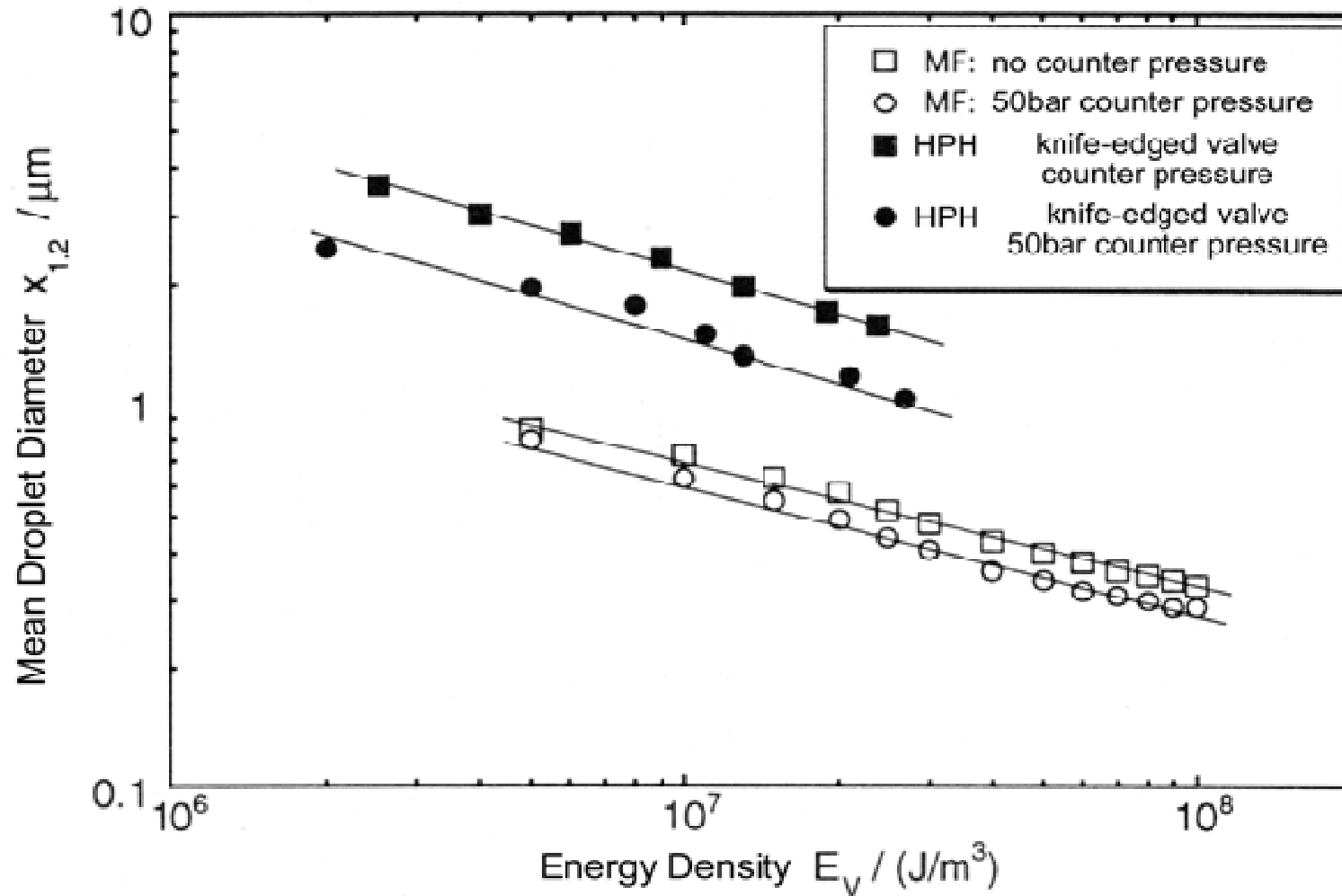


## From HPH to Microfluidizer (MF) A Small Design Change with a Large Effect



- In addition to pressure changes leading to cavitation, fluid jets also impinge in a mixing chamber
- Extremely turbulent flow situation and very high shear forces cause additional disruption of droplets
- Higher homogenization pressures possible
- NO MOVING PARTS! → low maintenance
- But: stronger possibility for blockage

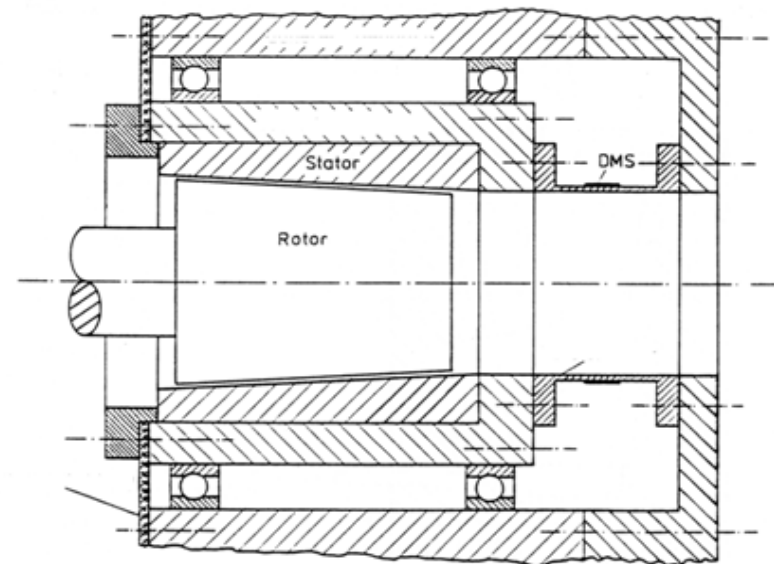
# HPH and MF Comparison





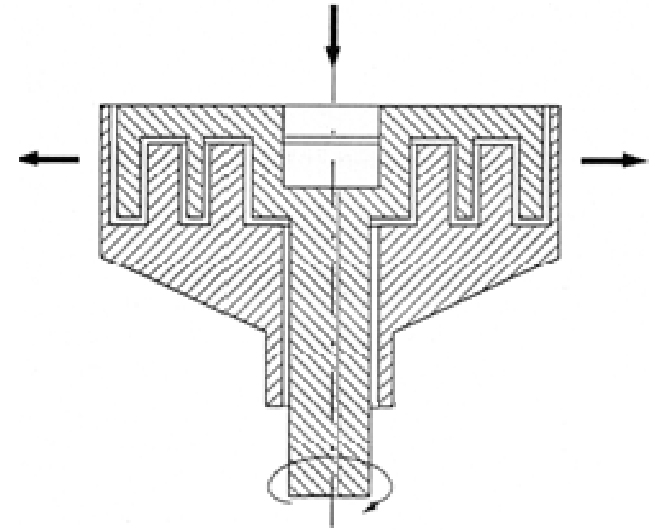
# III. Colloid Mills (CM)

- Droplet disruption in colloid mills occurs in a flow channel between a rotor-stator assembly
- The rotor may have a large variety of surface profiles (toothed)
- Typical rotational speeds are  $n=3000 \text{ min}^{-1}$
- Due to the conical design, the emulsions is transported without external pressure application
- The size of the gap alters residence time in the channel and exerted forces

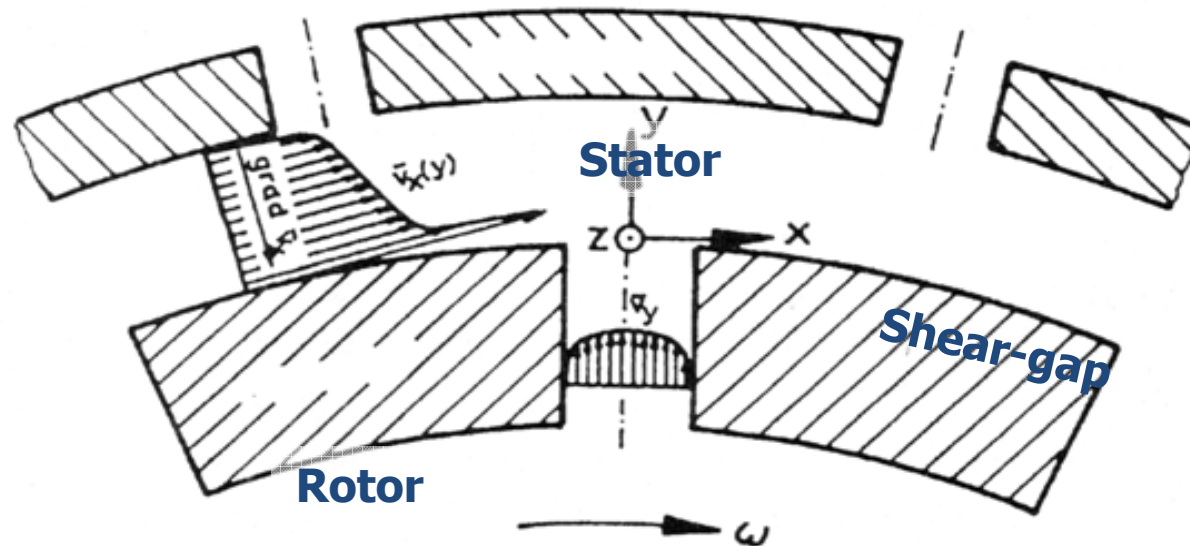


## IV: High Shear Disperser (HSD) – (Ultra) Turrax

- HSD or Ultra-Turrax Systems are rotor-stator systems similar to colloid mills
- They are composed of coaxial intermeshing rings with radial openings
- The fluid enters in the center of the systems and is accelerated by the rotor
- As it passes through the system, the fluid is accelerated and decelerated multiple times which results in high tangential forces
- Rotational speeds may be as high as  $n=20000 \text{ min}^{-1}$

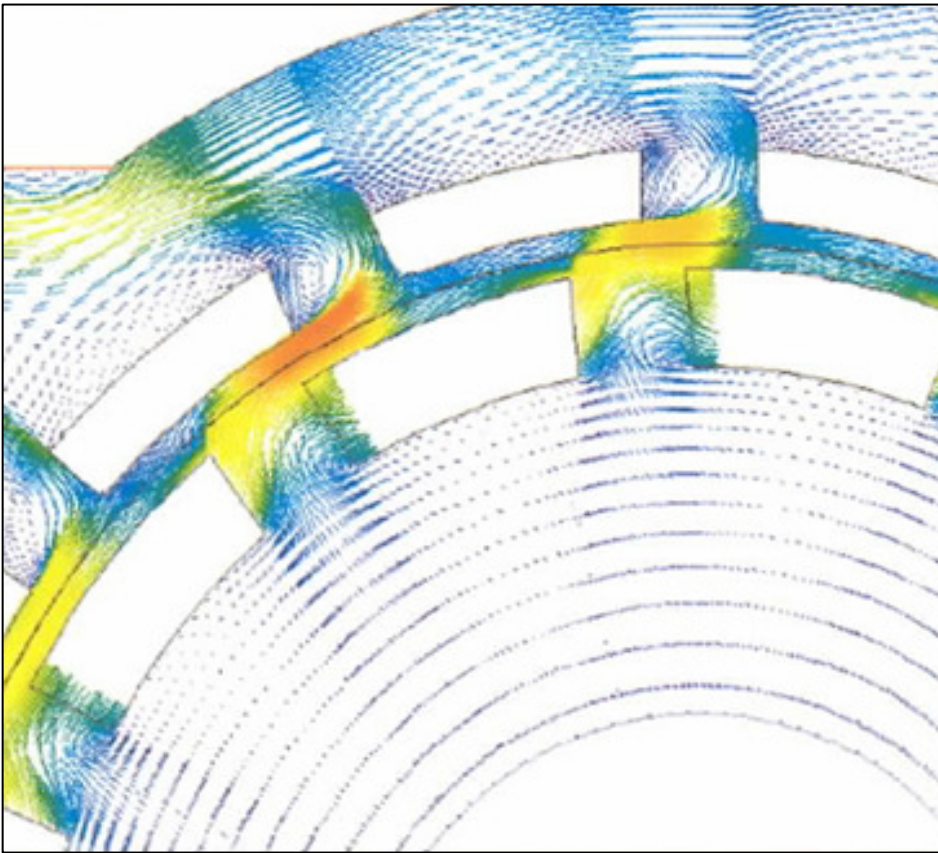


# High Shear Disperser (HSD): Principle of Droplet Disruption

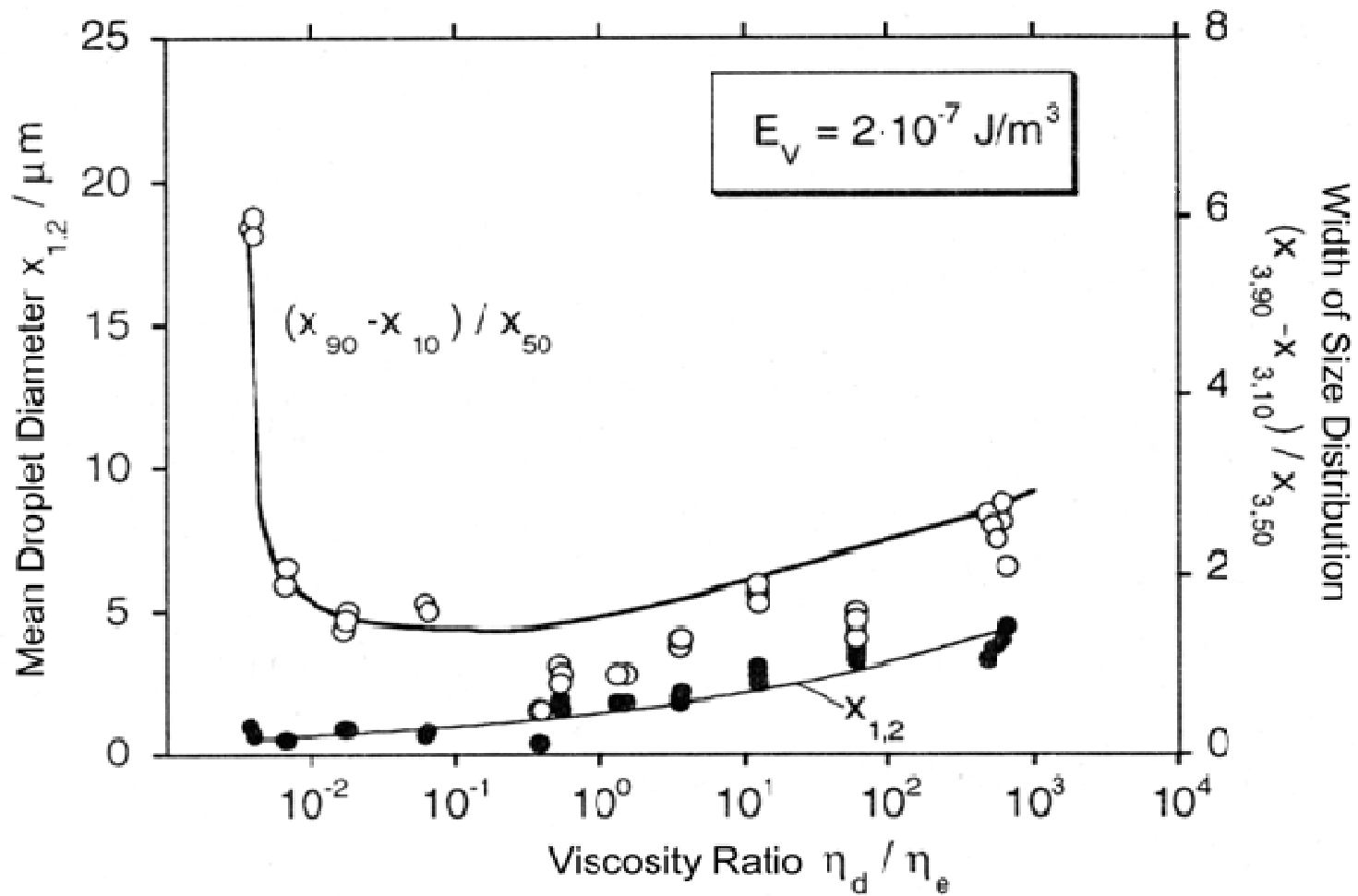


- The pre-emulsion is transported through the radial openings of the rotor systems and mixes with the liquid in the gap between the rotor and the stator
- High shear forces and turbulent flow situations arise that lead to a disruption of droplets

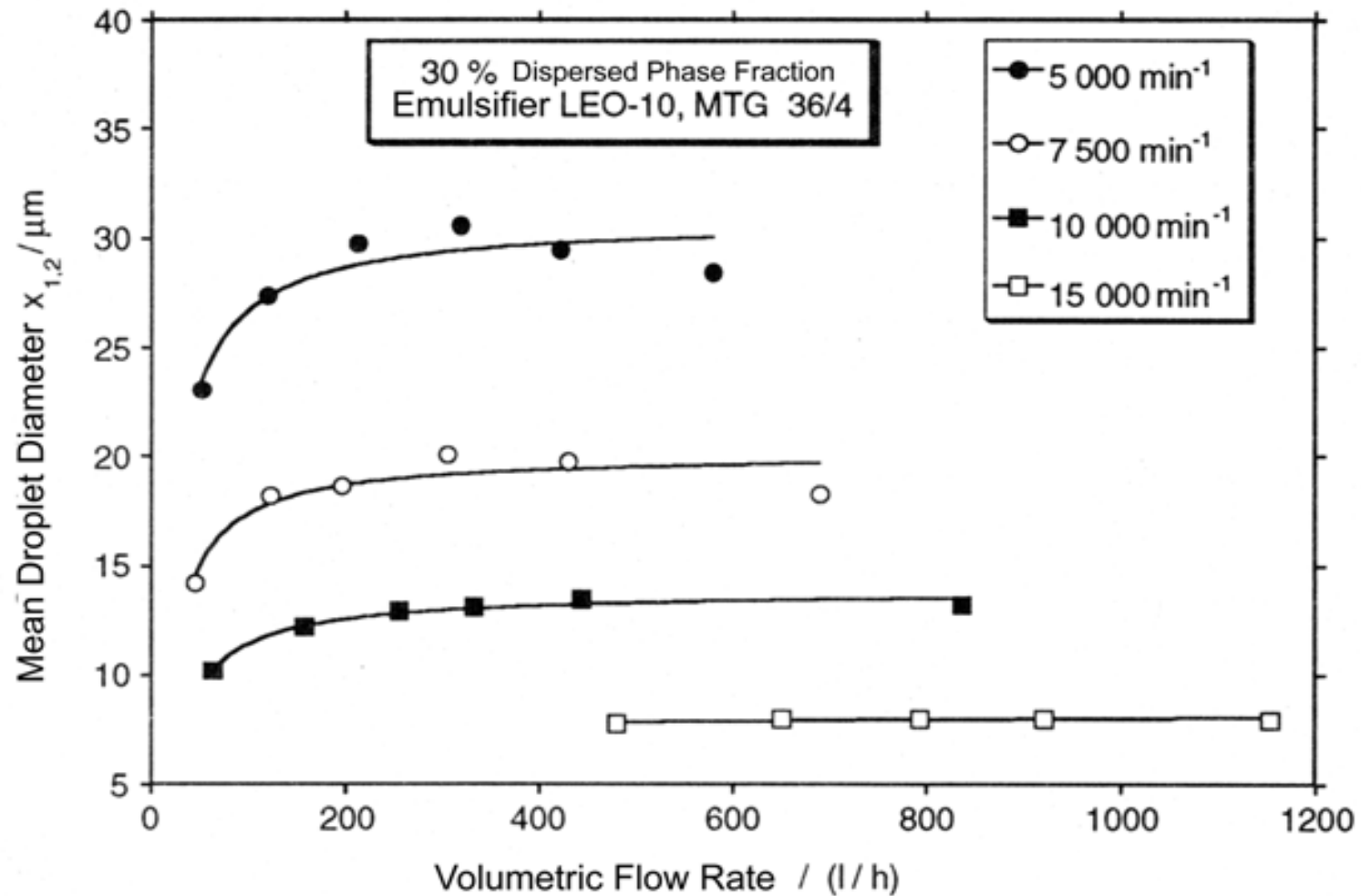
# HSD: Complexity of Flow Profiles



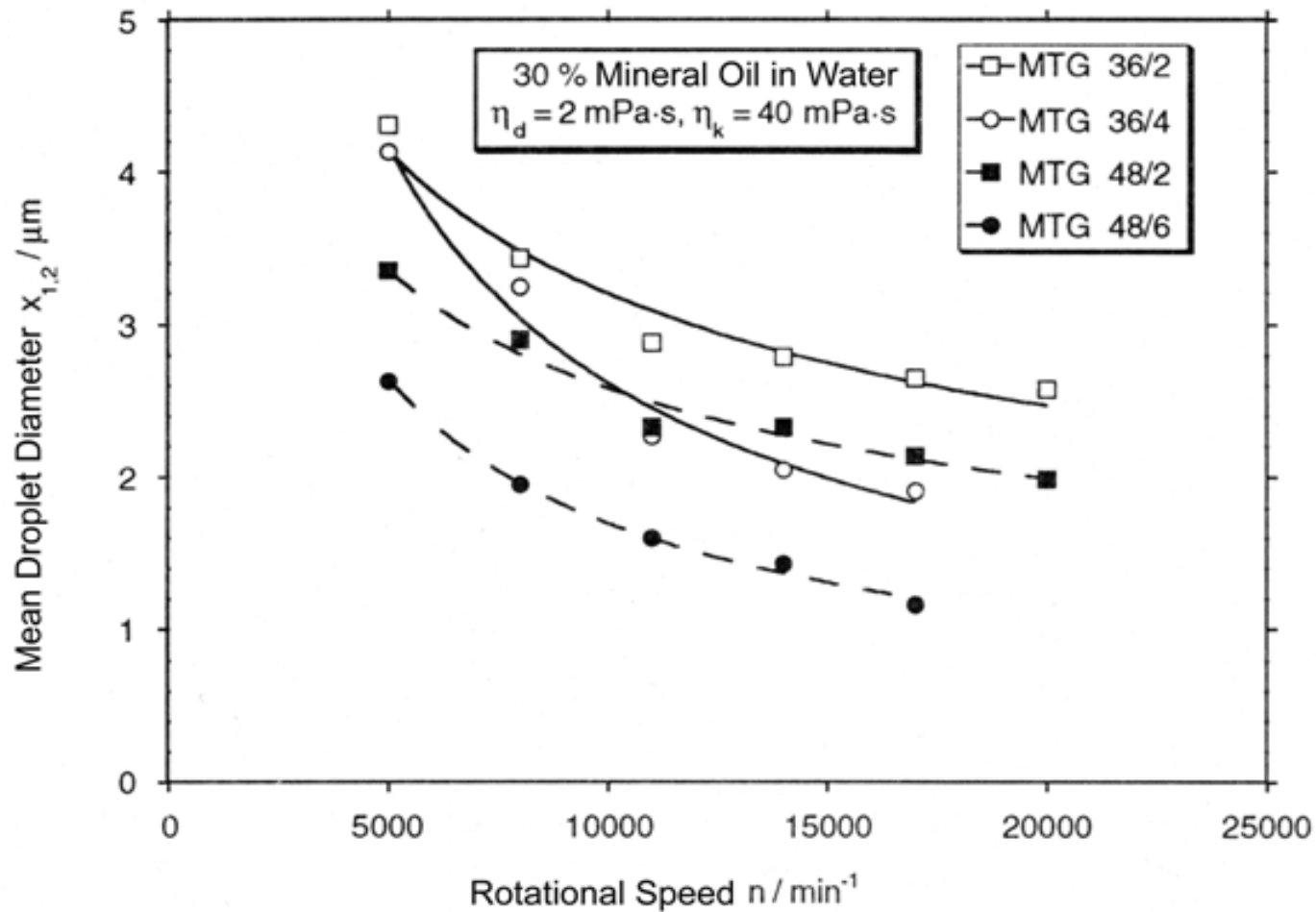
# HSD: Influence of Viscosity Ratio



# HSD: Influence of Residence Time

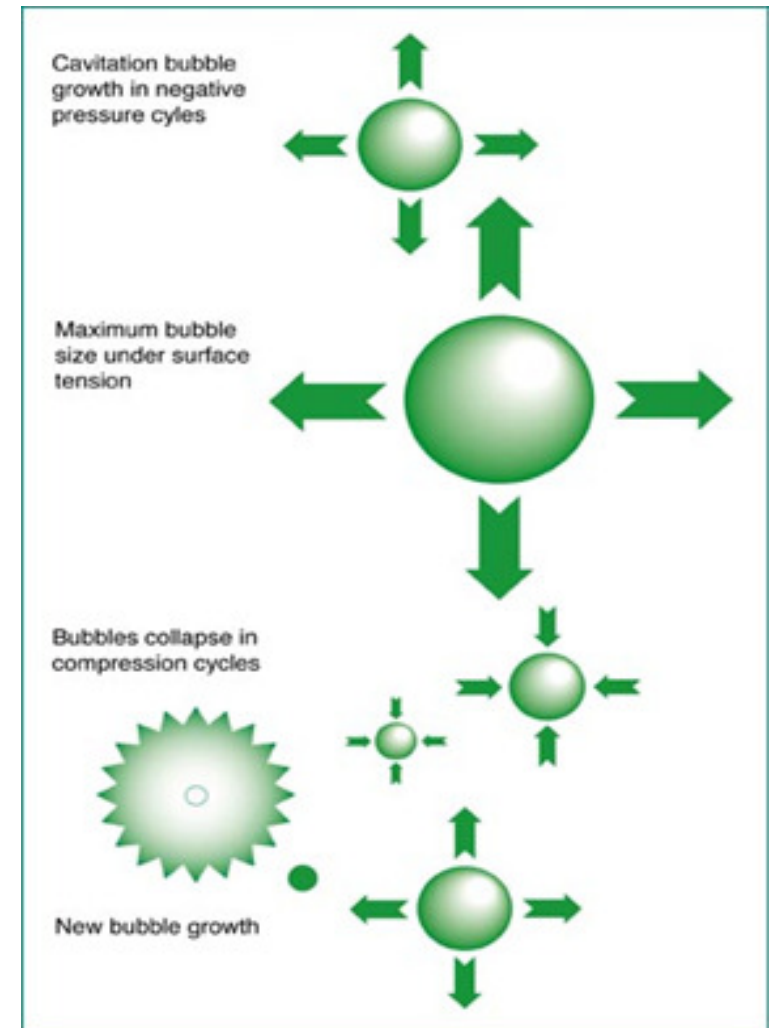


# HSD: Influence of Geometry of Rotor-Stator System



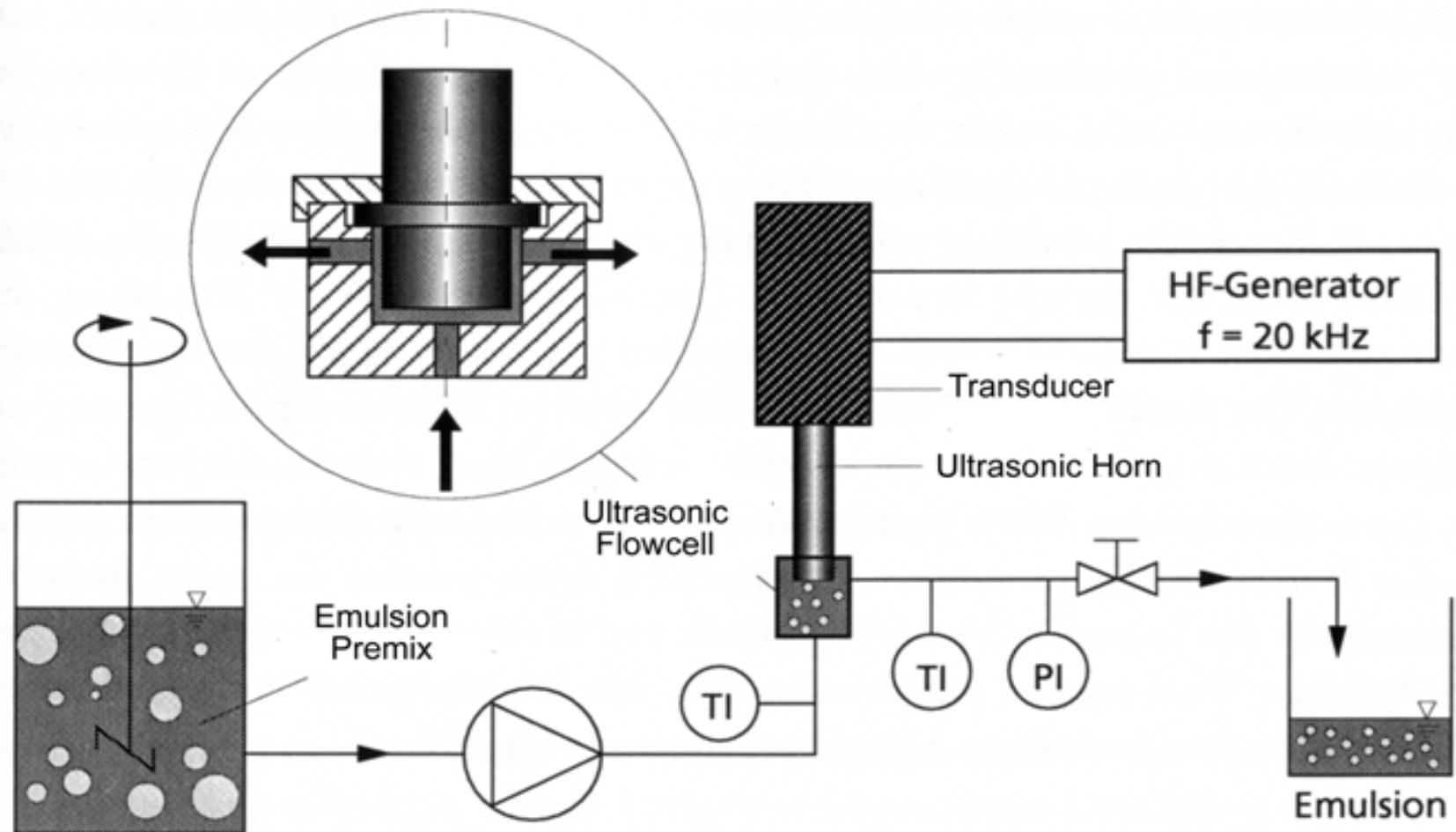
# V. Ultrasonic Homogenizer (UH)

- Piezo-electric or magneto-restrictive transducers generate sound waves with frequencies  $> 20$  kHz
- Associated pressure gradients cause deformation of droplets
- Cavitation caused by drop of local pressure below the vapor pressure of the solvent generates turbulent flow and high shear
- Can be run in batch or continuous using a flow cell





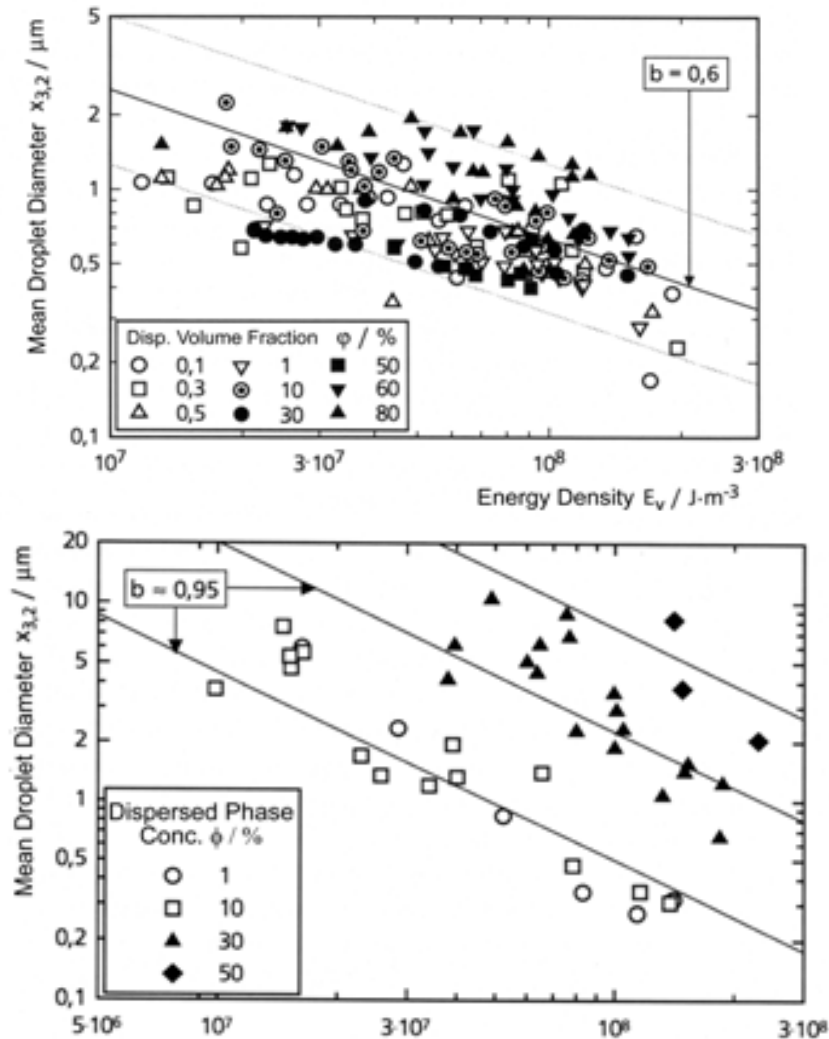
# Typical Design of a Continuous Ultrasonic Homogenizer



# Ultrasonic Homogenizer : Process Parameters

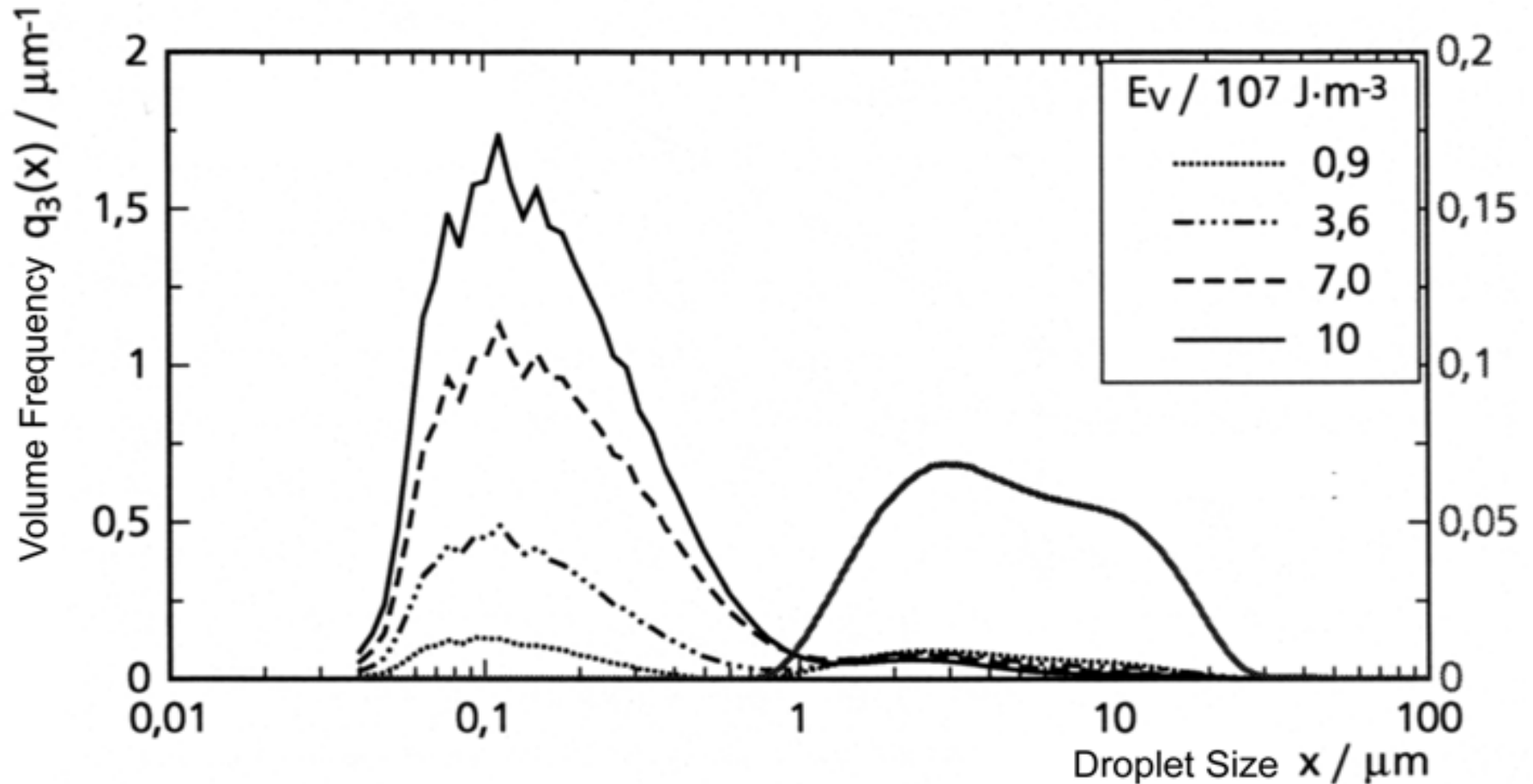
- **Frequency**
  - Size of cavitation bubbles decreases with increasing frequency
  - Wave intensity
  - A minimum pressure drop is required to initiate cavitation → below critical wave intensities, almost no droplet disruption
  - Above the critical pressure, direct relationship between applied intensity and achievable particle size
- **Sonication time**
  - Disruption and stabilization are kinetic events, thus, a minimum sonication time is required to achieve droplet disruption
- **Hydrostatic pressure**
  - Initially, improved emulsification (up to 5 bar), above 5 bar, decreased efficiency
- **Dissolved gas concentration**
  - Increased number of cavitation events but reduced intensity of cavitation collapse due to dampening
- **Viscosity & Temperature**
  - Influences droplet disruption

# Ultrasonic Homogenizer: Emulsifier Properties Play a Key Role

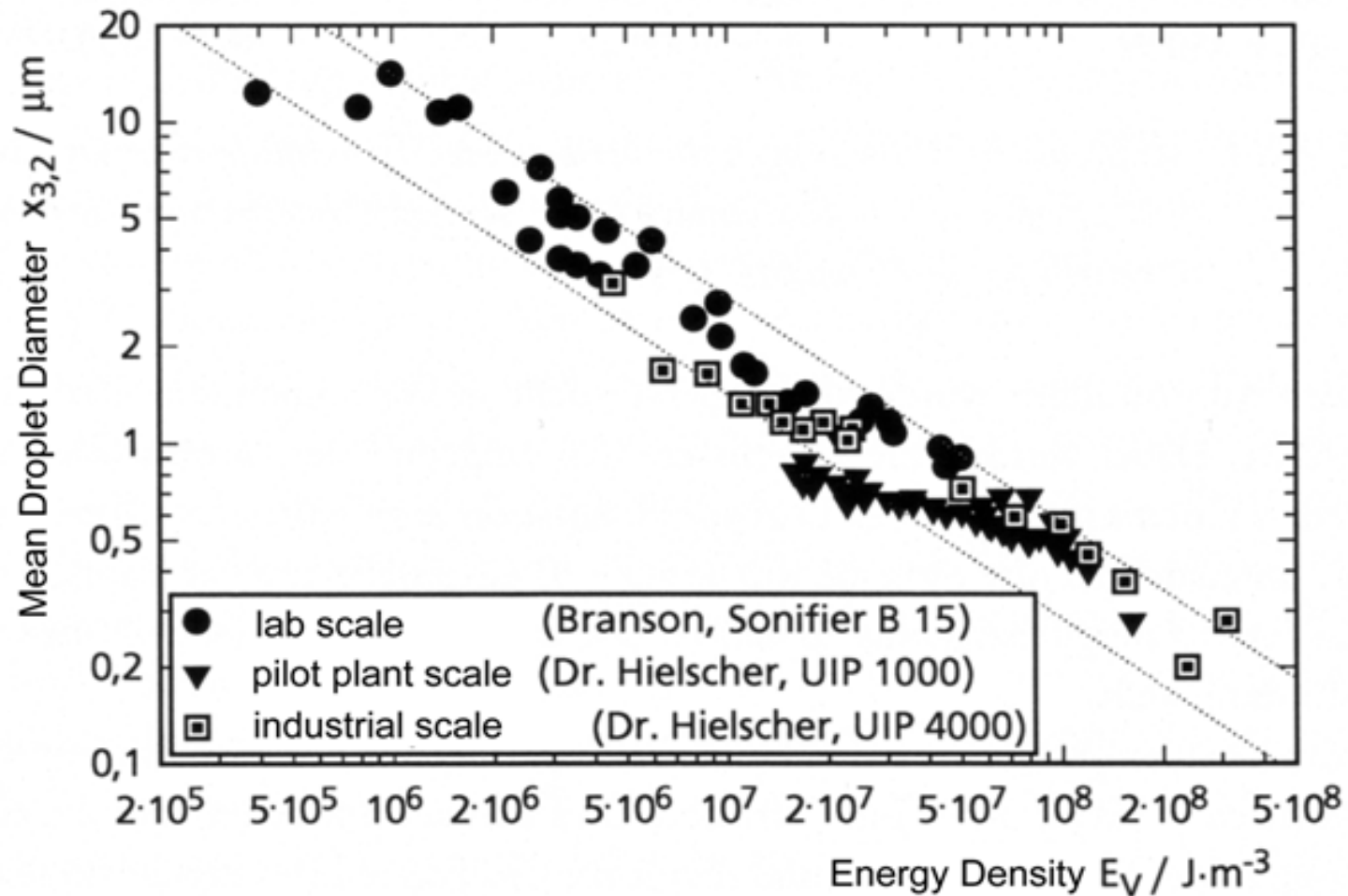


- The relationship between energy density, volume fraction and achievable mean droplet diameter depends strongly on the emulsifier.
- For slow emulsifiers (bottom), achievable particle sizes increase with increasing volume fraction
- For fast emulsifiers (top), smaller emulsion can be obtained even at high dispersed phase concentrations

# Ultrasonic Homogenizer: Peculiarity in Size Distribution Development

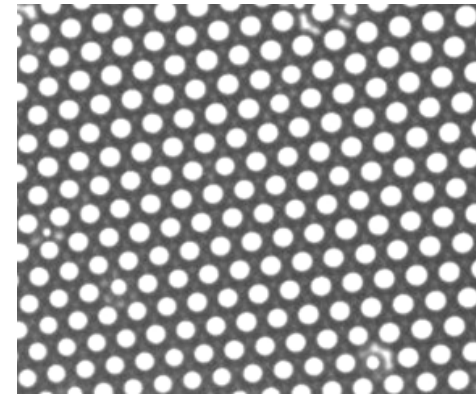
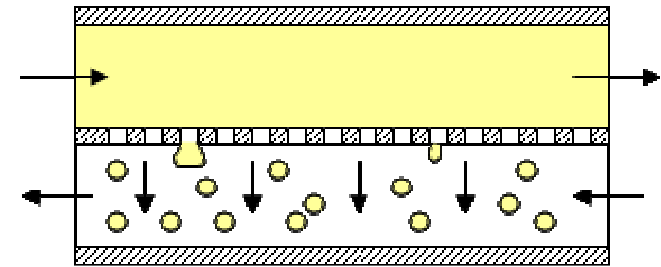


# Ultrasonic Homogenizer: Scale-up of Homogenizers



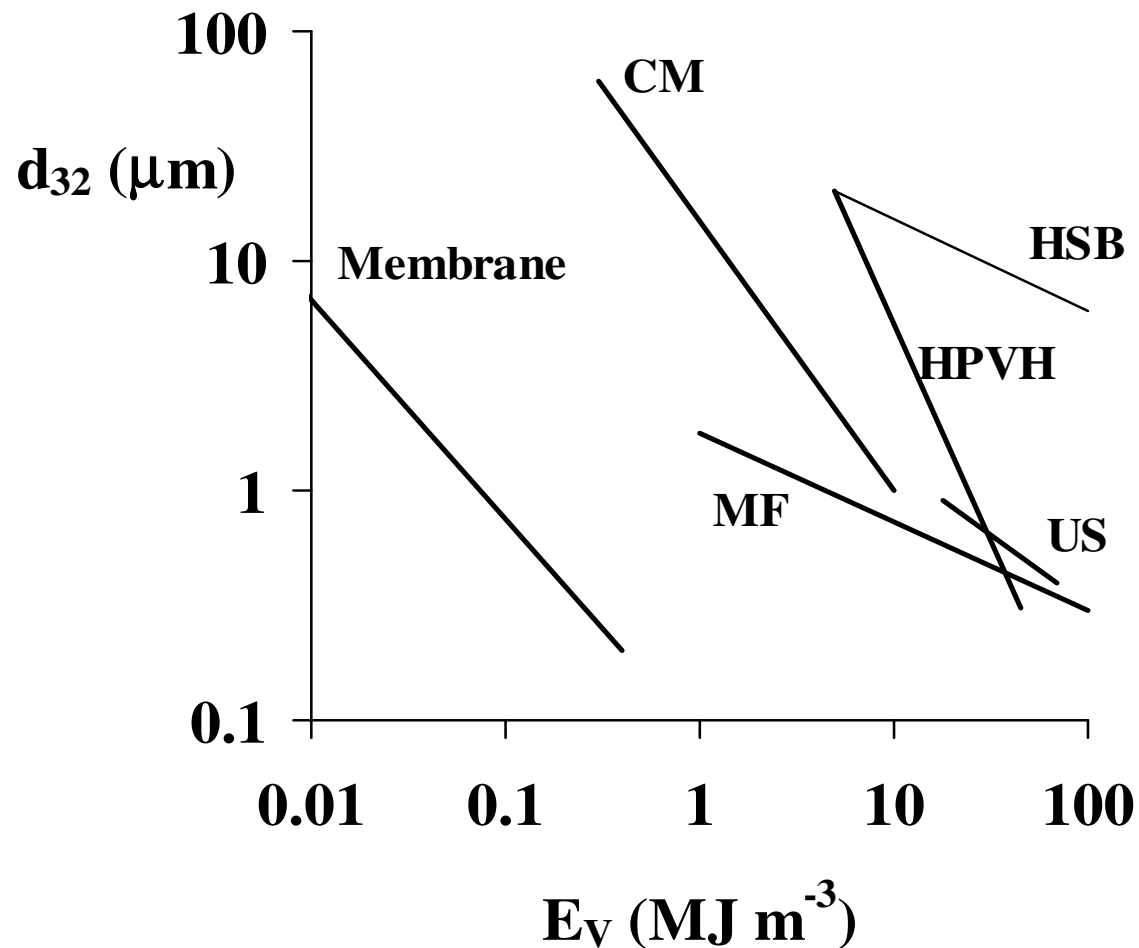
# VI. Membrane Homogenizers (MH)

- Dispersed phase or emulsion pushed through microporous membrane into continuous phase
- High energy efficiency
- Narrow particle size distribution possible
- Droplet size typically  $2-3 \times$  pore size
- For high dispersed phase concentrations, recirculation is needed  
→ time consuming
- Process parameters include:
  - Membrane pore size and material
  - Volume flow rates
  - Applied trans-membrane pressure
  - Others: temperature, viscosity, etc.



O/W Produced by Membrane

# Direct Comparison of Homogenizers

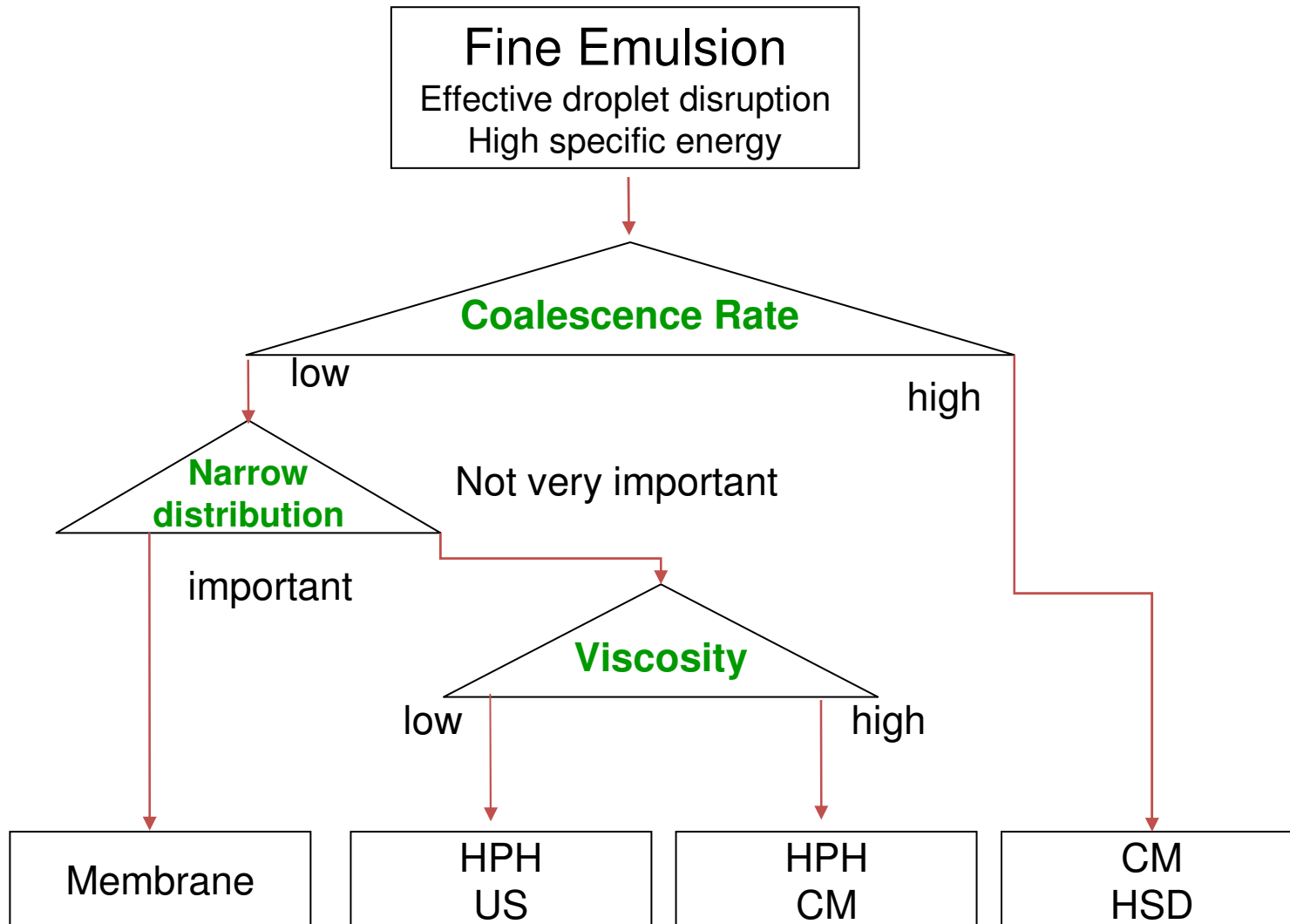


# Selecting a Homogenizer

- Define desired product characteristics
  - Particle size distribution, viscosity
- Define desired production conditions
  - Batch/Continuous, throughput, hygiene, temperature
- Identify, Test & Compare Homogenizers
  - High speed blender, high pressure valve, colloid mill, ultrasonic, membrane etc.
- Optimize Homogenization Conditions
  - Pressure, flow rate, rotation speed, time, temperature, emulsifier type, emulsifier concentration



# Which Homogenizer to Buy?



## Recap: Factors Affecting Droplet Size

- **Homogenizer**
  - Machine Parameters (Pressure, Rotation Speed, Time)
  - Energy Density
- **Component Phases**
  - Interfacial Tension
  - Viscosity
- **Emulsifier**
  - Adsorption Kinetics
  - Interfacial Tension Reduction
  - Stabilization of Droplets Against Aggregation